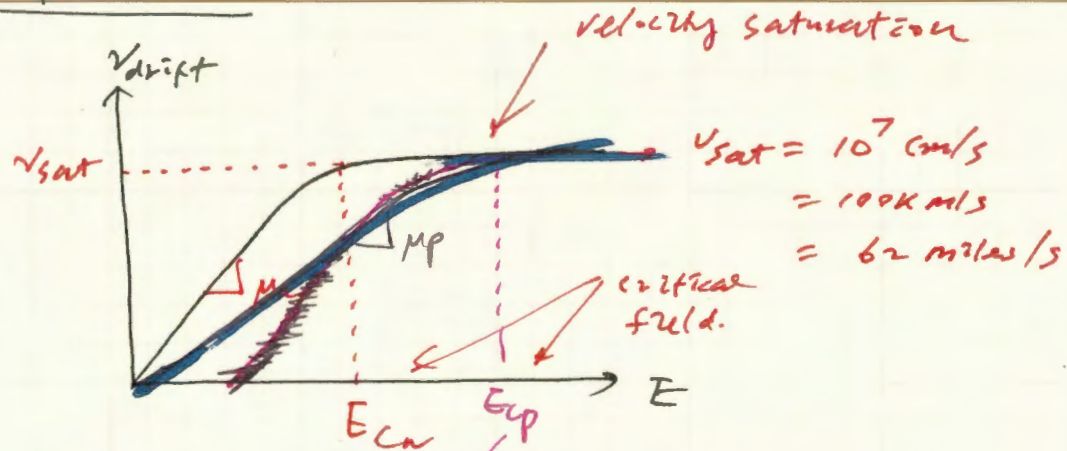
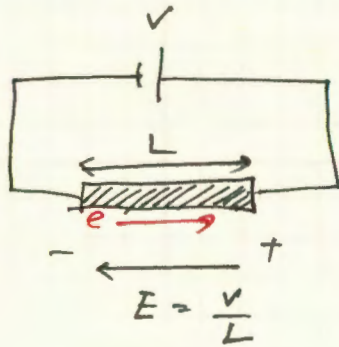


# Carrier velocity vs E-field



$$(*) \quad v_{drift} = \mu_n \frac{E}{1 + \frac{E}{E_c}}$$

$$\left\{ \begin{array}{l} \textcircled{i) \quad E \ll E_c, v_{drift} \approx \mu_n E \\ \textcircled{ii) \quad E \gg E_c, v_{drift} = \frac{1}{2} \mu_n E_c = v_{sat} \end{array} \right.$$

$$E_{cn} = 6 \times 10^4 \text{ V/cm (electron)} = 6 \text{ V/\mu m}$$

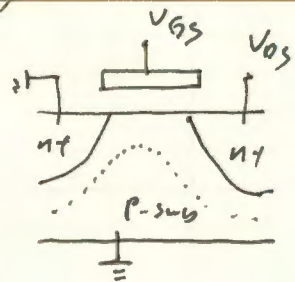
$$E_{cp} = 24 \times 10^4 \text{ V/cm (hole)} = 24 \text{ V/\mu m}$$

$$E_{cn} = 600 \text{ mV}/0.1 \mu\text{m} = 60 \text{ mV}/10 \text{ nm}$$

$$E_{cp} = 2.4 \text{ V}/0.1 \mu\text{m} = 240 \text{ mV}/10 \text{ nm}$$

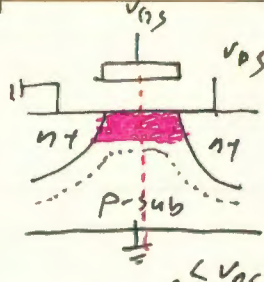
$$(*) \quad I_e = \frac{q}{b} \cdot v_{drift} \left\{ \begin{array}{l} \textcircled{i) \quad E \ll E_c, I_e = q \cdot \mu_n E \\ \textcircled{ii) \quad E \gg E_c, I_e = q \cdot v_{sat} \end{array} \right.$$

# ① Subthreshold



- $0 < V_{GS} < V_{th}$
  - No electron channel
  - Subthreshold current
- $$I_{DS} = I_S \left( e^{\frac{qV_{GS}}{kT}} - 1 \right) \left( 1 - e^{-\frac{qV_{DS}}{kT}} \right)$$

# ② Linear (= deep triode)



- $V_{GS} > V_{th}$ ,  $V_{DS} \ll V_{GS} - V_{th}$
  - Uniform electron channel
- $$Q_{ch1} = \frac{C_{ox}}{2} (V_{GS} - V_{th})$$
- $$Q_{ch2} = \frac{C_{ox}}{2} (V_{GD} - V_{th})$$
- $$V_{GD} = V_{GS} + V_{SD}$$
- $$= V_{GS} - V_{DS}$$
- $$\approx V_{GS}$$

$$Q_{ch1} \approx Q_{ch2}$$

$$② Q_T = Q_{ch1} + Q_{ch2}$$

$$= C_{ox} (V_{GS} - V_{th})$$

$$③ E = \frac{V_{DS}}{L}$$

$$④ I_{DS} = Q_T \cdot W \cdot \mu_n E$$

$$= \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th}) V_{DS}$$

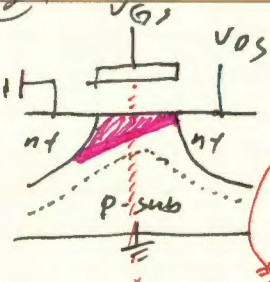
Linear

$$g_m = \frac{\partial I_{DS}}{\partial V_{GS}} = \mu_n C_{ox} \frac{W}{L} V_{DS}$$

$$g_{DS} = \frac{\partial I_{DS}}{\partial V_{DS}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})$$

$$r_o = \frac{1}{g_{DS}} = \frac{1}{\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})}$$

# ③ Triode



- $V_{GS} > V_{th}$ ,  $V_{DS} \approx V_{GS} - V_{th}$
  - Non-uniform electron channel
- $$Q_{ch1} = \frac{C_{ox}}{2} (V_{GS} - V_{th})$$
- $$Q_{ch2} = \frac{C_{ox}}{2} (V_{GD} - V_{th})$$
- $$= \frac{C_{ox}}{2} (V_{GS} - V_{DS} - V_{th})$$
- $$Q_T = Q_{ch1} + Q_{ch2}$$
- $$= C_{ox} (V_{GS} - V_{th} - \frac{1}{2} V_{DS})$$

$$E = \frac{V_{DS}}{L}$$

$$I_{DS} = Q_T \cdot W \cdot \mu_n E$$

$$= \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th} - \frac{1}{2} V_{DS}) V_{DS}$$

Parabolic

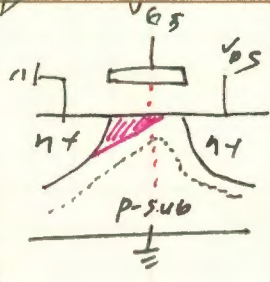
$$g_m = \mu_n C_{ox} \frac{W}{L} V_{DS}$$

$g_{DS}, r_o \Rightarrow$  Non-linear

$$V_{DS, sat} = V_{GS} - V_{th}$$

$$= \sqrt{\frac{2 I_{DS}}{\mu_n C_{ox} \frac{W}{L}}}$$

# ④ Saturation (Long channel approximation)



- $V_{GS} > V_{th}$ ,  $V_{DS} > V_{GS} - V_{th}$
- pinch-off in electron channel

$$Q_{ch1} = \frac{C_{ox}}{2} (V_{GS} - V_{th})$$

$$Q_{ch2} \approx 0$$

$$Q_T = Q_{ch1}$$

$$= \frac{C_{ox}}{2} (V_{GS} - V_{th})$$

$$E = \frac{V_{GS} - V_{th}}{L}$$

channel length modulation

$$I_{DS} = Q_T \cdot W \cdot \mu_n E$$

$$= \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})^2$$

$$\approx \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})^2 (1 + \lambda V_{DS})$$

$$g_m = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})$$

channel length mod. factor

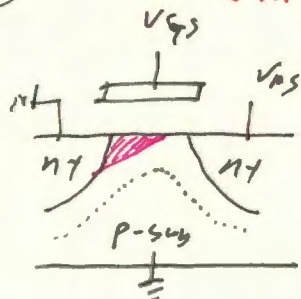
$$= \sqrt{2 \mu_n C_{ox} \frac{W}{L} I_{DS}}$$

$$= \frac{2 I_{DS}}{V_{GS} - V_{th}}$$

$$r_o = \frac{1}{\lambda I_{DS}}$$



⑤ Velocity saturation (short channel effect)



- $V_{GS} > V_{th}$ ,  $V_{DS} > V_{GS} - V_{th}$
- pinch off in electron channel

$$Q_{ch1} = \frac{C_{ox}}{2} (V_{GS} - V_{th})$$

$$Q_{ch2} = 0$$

$$Q_T \approx Q_{ch1}$$

$$E = \frac{V_{GS} - V_{th}}{L'} > E_c$$

$$I_{DS} = Q_T \cdot W \cdot \mu_n E_c$$

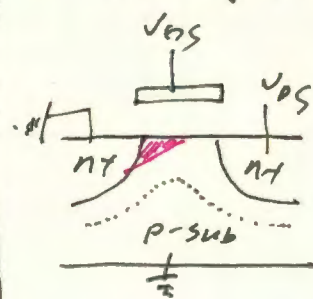
$$= \frac{C_{ox} \cdot W}{2} (V_{GS} - V_{th}) \mu_n E_c$$

$$= C_{ox} \cdot W (V_{GS} - V_{th}) v_{sat}$$

$$g_m = C_{ox} \cdot W \cdot v_{sat}$$

$\Rightarrow$  No dependent on  $L$

⑥ General saturation model including short channel effect.



- $V_{GS} > V_{th}$ ,  $V_{DS} > V_{GS} - V_{th}$
- pinch off in electron channel

$$Q_{ch1} = \frac{C_{ox}}{2} (V_{GS} - V_{th})$$

$$Q_{ch2} = 0$$

$$Q_T = Q_{ch1}$$

$$E = \frac{V_{GS} - V_{th}}{L'} < E_c$$

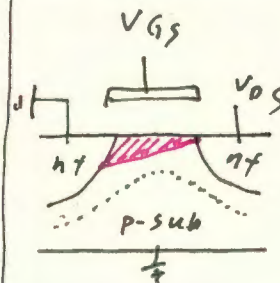
$$I_{DS} = Q_T \cdot W \left( \mu_n \frac{E}{1 + \frac{E}{E_c}} \right)$$

$$= \frac{1}{2} \mu_n C_{ox} \frac{W}{L'} (V_{GS} - V_{th})^2 \left( \frac{1}{1 + \frac{V_{GS} - V_{th}}{E_c \cdot L'}} \right)$$

At  $V_{DS} = V_{DS,sat}$  these two current is same.

$$V_{DS,sat} = (V_{GS} - V_{th})$$

⑦ General triode model including short channel effect



- $V_{GS} > V_{th}$ ,  $V_{DS} \leq V_{GS} - V_{th}$
- Non-uniform electron channel

$$Q_{ch1} = \frac{C_{ox}}{2} (V_{GS} - V_{th})$$

$$Q_{ch2} = \frac{C_{ox}}{2} (V_{GS} - V_{th}) = \frac{C_{ox}}{2} (V_{GS} - V_{DS} - V_{th})$$

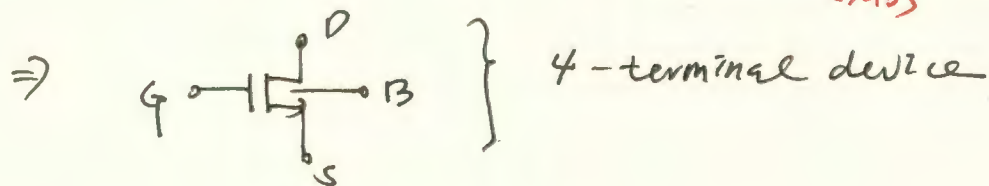
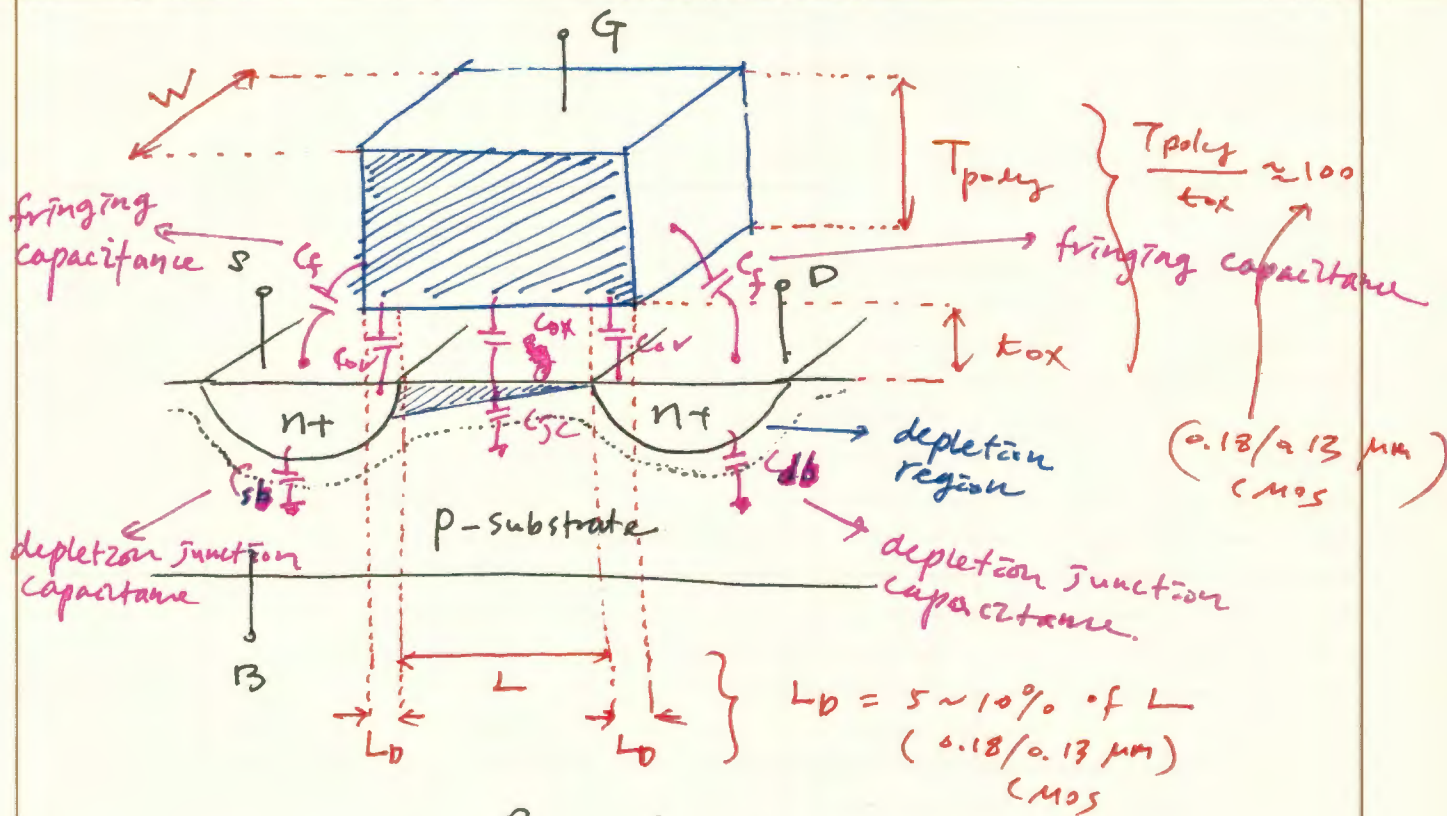
$$Q_T = Q_{ch1} + Q_{ch2}$$

$$= C_{ox} (V_{GS} - V_{th} - \frac{1}{2} V_{DS})$$

$$E = \frac{V_{DS}}{L}$$

$$I_{DS} = Q_T \cdot W \cdot \left( \mu_n \frac{E}{1 + \frac{E}{E_c}} \right)$$

$$= \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th} - \frac{1}{2} V_{DS}) \left( \frac{V_{DS}}{1 + \frac{V_{DS}}{E_c \cdot L}} \right)$$



⇒  $L_D$  is extra extension of gate metal (poly silicon) to ~~gate~~ source and drain region to prevent channel discontinuity

⇒ Overlap capacitance

$$C_{ov} = C_{ox} \cdot W \cdot L_D$$

oxide capacitance,  $C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$  per unit area

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}} = \frac{\epsilon_0 \epsilon_r}{t_{ox}}$$

$$8.854 \times 10^{-14} \text{ F/cm}$$

4 for SiO<sub>2</sub>

⇒  $C_g \approx$  constant for process generations

(2A)  $L = 5 \mu\text{m}$   
 $t_{ox} = 1100 \text{ Å}$

$L = 0.35 \mu\text{m}$   
 $t_{ox} = 75 \text{ Å}$

$L = 0.18 \mu\text{m}$   
 $t_{ox} = 35 \text{ Å}$

$L = 0.13 \mu\text{m}$   
 $t_{ox} = 22 \text{ Å}$

	0.18 μm NMOS	0.13 μm NMOS
L	0.18 μm	0.13 μm
t <sub>ox</sub>	35 Å	22 Å
C <sub>ox</sub>	10 fF/μm <sup>2</sup>	16 fF/μm <sup>2</sup>
C <sub>gate</sub>	<del>10 fF/μm</del>	

$$C_g = C_{ox} \cdot W \cdot L = (C_{ox} \cdot L) \cdot W = C_g \cdot W$$

$C_g \approx 2 \text{ fF/μm}$

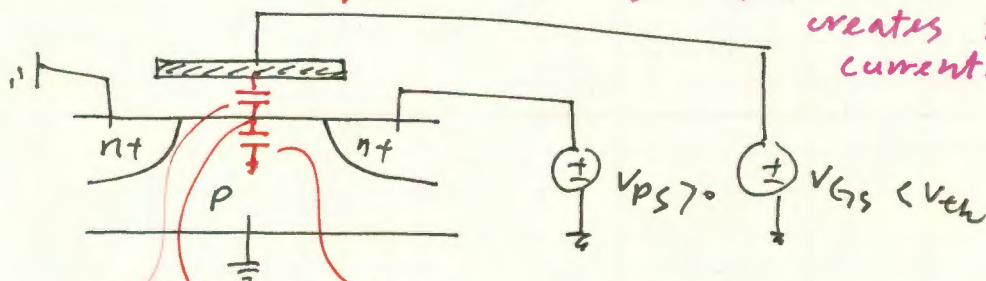


## \* I-V characteristics

①  $0 < V_{GS} < V_{th}$ ,  $V_{DS} > 0$

⇒ Subthreshold region

No electron channel but lateral bipolar NPN creates subthreshold current.



Can be used for ultra-low-power systems. (ex digital watch Bio-medical systems).

$V_{surface} = \text{Surface potential voltage}$   
 $= V_{GS} \times \frac{C_{ox}}{C_{ox} + C_{dep}}$

⇒  $V_{GS}$  depletes holes at the surface of P-substrate under gate area.

⇒ This creates a depletion capacitance,  $C_{dep}$

⇒ Surface voltage,  $V_{surface} = V_{GS} \cdot \frac{C_{ox}}{C_{ox} + C_{dep}} = V_{GS} \cdot \frac{1}{1 + \frac{C_{dep}}{C_{ox}}} = \frac{V_{GS}}{n}$

This gm can be larger than standard gm of saturation mode.

⇒  $V_{surface}$  will be developed on the surface of P-substrate.

⇒ This forms N-P-N transistor (lateral bipolar transistor)

$$I_{DS} = I_S \left( e^{\frac{V_{GS}}{nV_T}} - 1 \right) \left( 1 - e^{-\frac{V_{DS}}{V_T}} \right)$$

NOTE: (if  $V_{DS} \gg V_T$ )

①  $g_m$  (current driving capability)

$$= \frac{\partial I_{DS}}{\partial V_{GS}} \approx \frac{I_S}{nV_T} \frac{V_{GS}}{e^{nV_T}} - n = 1 + \frac{C_{dep}}{C_{ox}}$$

② No base current

$I_S = \text{Reverse saturation current}$

⇒ Subthreshold Current.

leakage current typically nA, pA order, could cause standby power dissipation in VLSI systems

~~$I_{DS} \approx I_S \approx \text{pA} \sim \text{nA}$~~

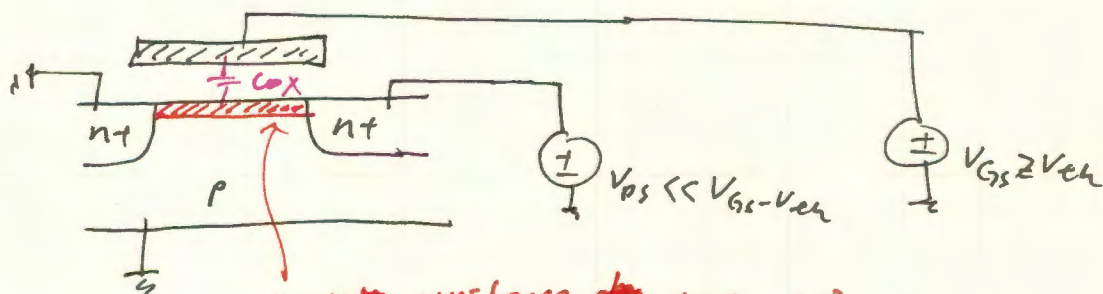
③  $V_{GS} \gg V_{th}$ ,  $V_{DS} \ll V_{GS} - V_{th}$

$\Rightarrow$  linear region

$\Rightarrow V_D - V_S \ll V_G - V_S - V_{th}$

$\Rightarrow V_{th} \ll V_G - V_D$

$\Rightarrow V_{th} \ll V_{GD}$



nearly-uniform electron channel (why?)  
 driving voltage

$\Rightarrow$  channel charge per unit area

channel charge per unit length

$Q_{ch} = -(V_{GS} - V_{th}) C_{ox}$

$Q_{ch} = -(V_{GS} - V_{th}) C_{ox} \cdot W$

oxide capacitance per unit area

$\Rightarrow I_{DS} = Q_{ch} \cdot V_{drift}$

$= -Q_{ch} \mu_n E$

$= -Q_{ch} \mu_n \frac{V_{DS}}{L}$

$= \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th}) V_{DS}$

electron drift velocity

$V_{drift} = -\mu_n E$

$= -\mu_n \left( \frac{V}{L} \right)$

$\mu_n$ : electron mobility

$E$ : applied E-field

$V$ : applied voltage

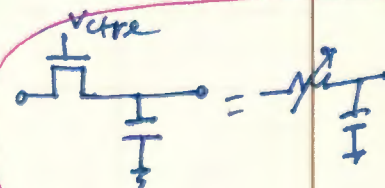
$L$ : length

$\Rightarrow g_m = \frac{\partial I_{DS}}{\partial V_{GS}} = \mu_n C_{ox} \frac{W}{L} V_{DS}$

$\Rightarrow I_{DS} - V_{DS}$ : linear relationship

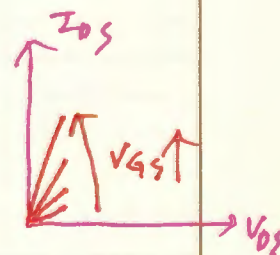
$\Rightarrow$  linear region

$\Rightarrow R_{DS} = \frac{V_{DS}}{I_{DS}} = \frac{1}{\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})}$



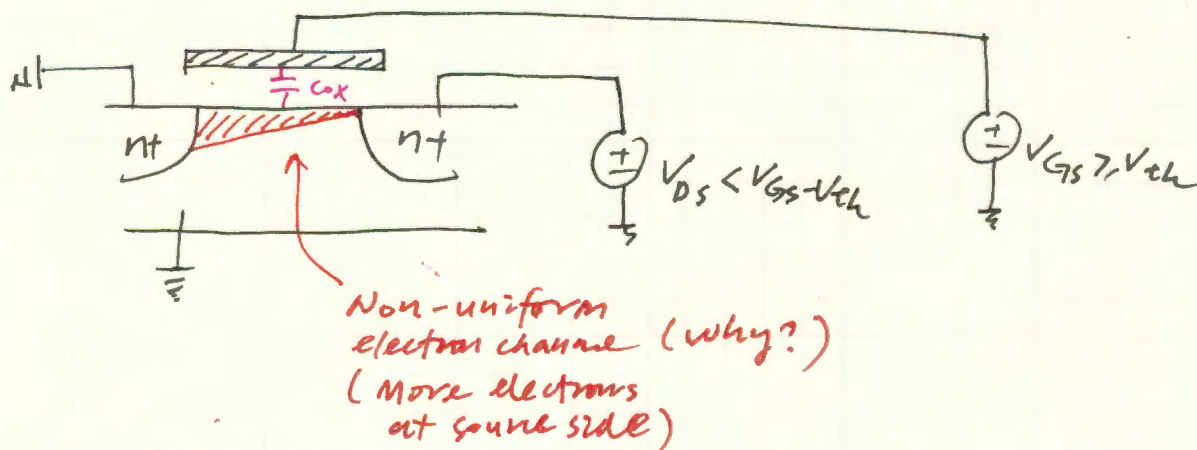
① NOTE: The electron channel is a linear resistor.

②  $R_{DS}$  can be controlled by  $V_{GS}$   
 $\Rightarrow$  voltage controlled resistor.





③  $V_{GS} > V_{th}$  ,  $V_{DS} < V_{GS} - V_{th}$   
 $\Rightarrow$  triode region  $\Rightarrow V_D - V_S < V_G - V_S - V_{th}$   
 $\Rightarrow V_{th} < V_G - V_D$   
 $\Rightarrow \boxed{V_{th} < V_{GD}}$



$\Rightarrow$  channel charge approximation  
 ① channel charge at source side is determined by  $(V_{GS} - V_{th})$ .

$$\therefore Q_{ch1} = -\frac{C_{ox}}{2} (V_{GS} - V_{th})$$

② channel charge at drain side is determined by  $(V_{GD} - V_{th})$

$$\therefore Q_{ch2} = -\frac{C_{ox}}{2} (V_{GD} - V_{th})$$

③ total channel charge per unit ~~channel~~ area

$$Q_{ch} = Q_{ch1} + Q_{ch2}$$

$$= -\frac{C_{ox}}{2} (V_{GS} + V_{GD} - 2V_{th})$$

$$= -\frac{C_{ox}}{2} (V_{GS} + V_{GS} + V_{SD} - 2V_{th})$$

$$= -\frac{C_{ox}}{2} (2V_{GS} - 2V_{th} - V_{DS})$$

$$= -C_{ox} (V_{GS} - V_{th} - \frac{1}{2}V_{DS})$$

④ Total channel charge per unit length

$$Q'_{ch} = -C_{ox} W (V_{GS} - V_{th} - \frac{1}{2}V_{DS})$$

$$\Rightarrow I_{DS} = -Q_{ch} \cdot v_{avt}$$

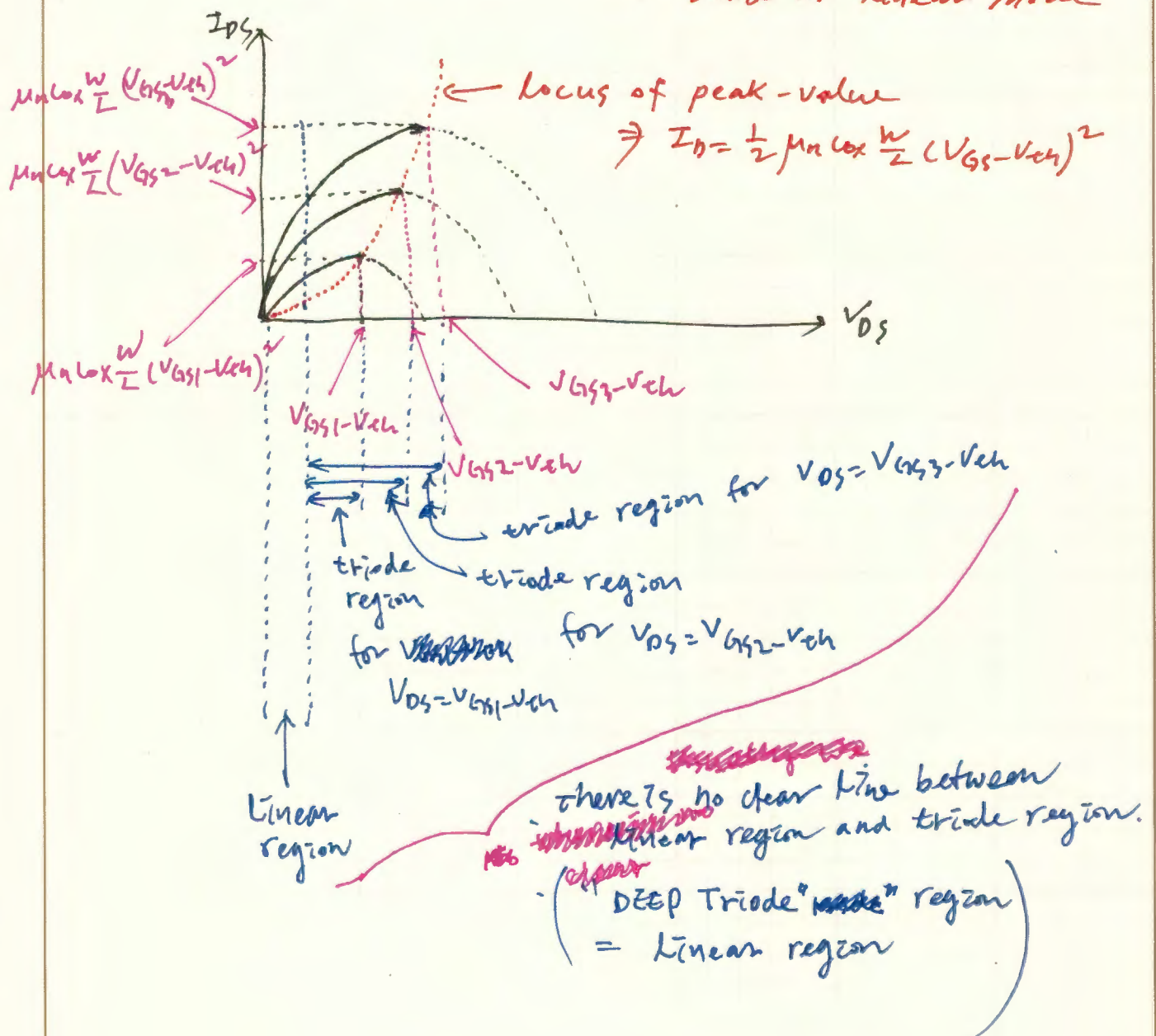
$$= -Q_{ch} \cdot \mu_n E$$

$$= -Q_{ch} \cdot \mu_n \frac{V_{DS}}{L}$$

$$= \mu_n \epsilon_{ox} \frac{W}{L} (V_{GS} - V_{th} - \frac{1}{2} V_{DS}) V_{DS}$$

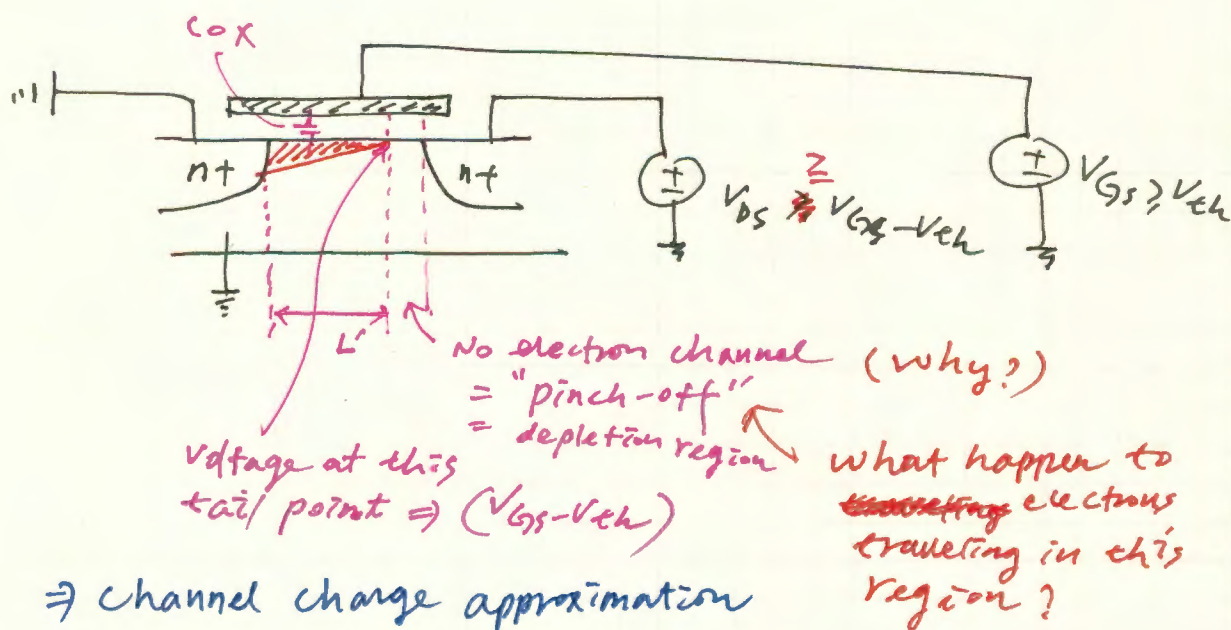
$$= \mu_n \epsilon_{ox} \frac{W}{L} \left( (V_{GS} - V_{th}) V_{DS} - \frac{1}{2} V_{DS}^2 \right)$$

(+)  $V_{DS} \ll V_{GS} - V_{th} \rightarrow I_{DS} = \mu_n \epsilon_{ox} \frac{W}{L} (V_{GS} - V_{th}) V_{DS}$   
 $\rightarrow$  same as linear mode





④  $V_{GS} \geq V_{th}$ ,  $V_{DS} \geq V_{GS} - V_{th}$   
 $\Rightarrow V_D - V_S \geq V_G - V_S - V_{th}$   
 $\Rightarrow V_{th} \geq V_G - V_D$   
 $\Rightarrow V_{th} \geq V_{GP}$



$\Rightarrow$  channel charge approximation

- ① channel charge at source side is determined by  $(V_{GS} - V_{th})$ .

$$\therefore Q_{ch1} = -\frac{C_{ox}}{2} (V_{GS} - V_{th})$$

- ② channel charge at drain side is negligible

- ③ total channel charge per unit area

$$Q_{ch} = Q_{ch1} = -\frac{C_{ox}}{2} (V_{GS} - V_{th})$$

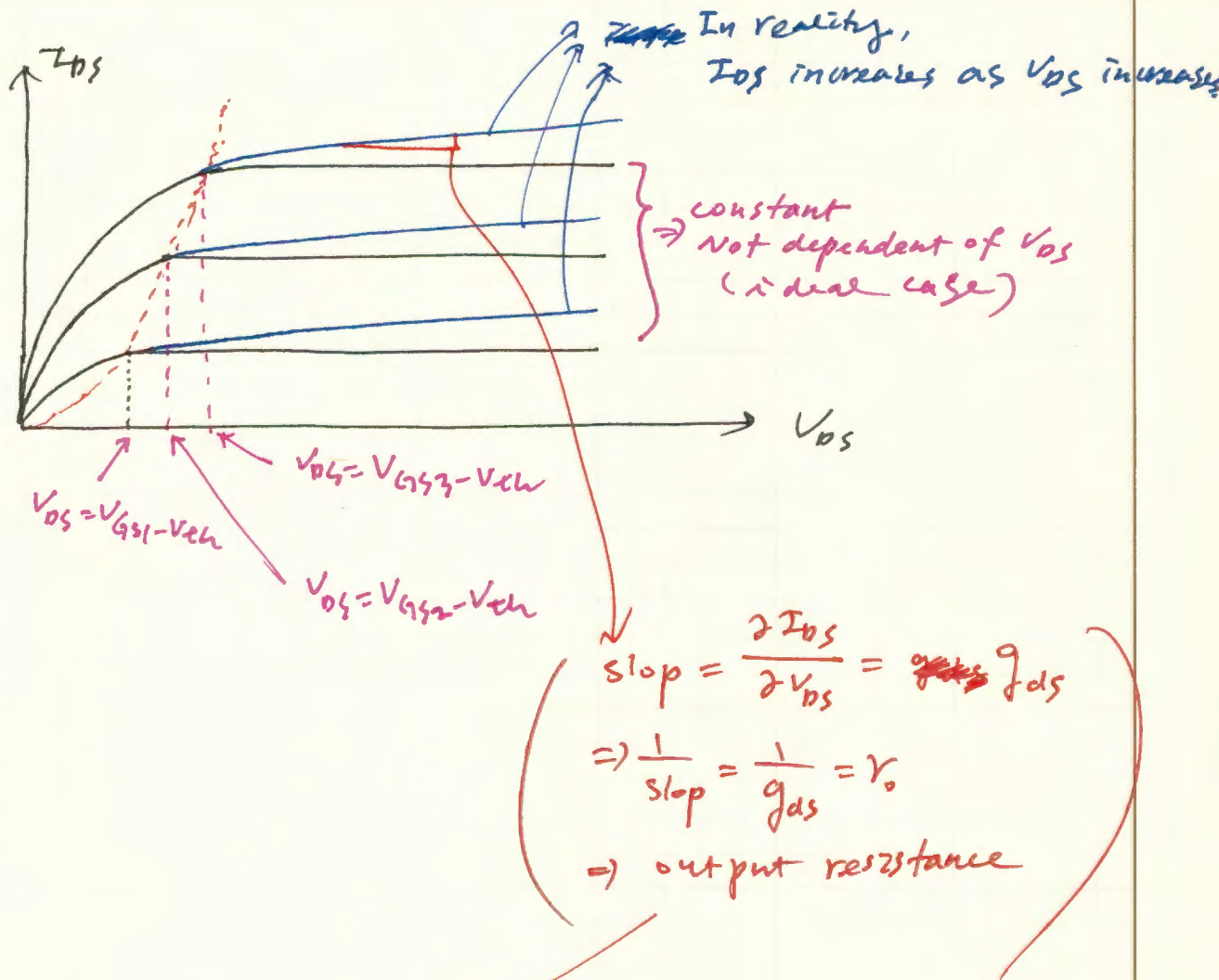
- ④ total channel charge per unit length

$$Q'_{ch} = -\frac{C_{ox}}{2} \cdot W (V_{GS} - V_{th})$$

$$\Rightarrow I_{DS} = -Q'_{ch} \cdot v_{drift} = -Q'_{ch} \cdot \mu_n E = -Q'_{ch} \mu_n \frac{V_{GS} - V_{th}}{L'}$$

$$= \frac{1}{2} \mu_n C_{ox} \frac{W}{L'} (V_{GS} - V_{th})^2$$

$$\approx \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})^2 \quad \text{approximation } L \approx L'$$



⊗ As  $V_{DS}$  increases, effective electron <sup>drift</sup> ~~moving~~ distance,  $L'$ , will be decreases

$\Rightarrow$  effective channel length decreases

$\Rightarrow$  channel-length modulation

$\Rightarrow$  As  $V_{DS} \uparrow \leadsto I_{DS} \uparrow$

⊗ 
$$I_{DS} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})^2 (1 + \lambda V_{DS})$$

$\Rightarrow \frac{1}{\lambda I_{DS}} = r_o$

$\Rightarrow \lambda = \frac{1}{r_o I_{DS}}$

channel-length modulation factor



### \* I-V characteristics

① Linear region ( $V_{DS} \ll V_{GS} - V_{th}$ )

$$I_{DS} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th}) V_{DS}$$

② triode region ( $V_{DS} < V_{GS} - V_{th}$ )

$$I_{DS} = \mu_n C_{ox} \frac{W}{L} \left( (V_{GS} - V_{th}) V_{DS} - \frac{1}{2} V_{DS}^2 \right)$$

③ saturation region ( $V_{DS} \geq V_{GS} - V_{th}$ )

$$I_{DS} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})^2$$

④ saturation region with channel-length modulation

$$I_{DS} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})^2 (1 + \lambda V_{DS})$$

\* transconductance

$$g_m = \frac{\partial I_{DS}}{\partial V_{GS}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{th})$$

$$= \sqrt{2 \mu_n C_{ox} \frac{W}{L} I_{DS}}$$

$$= \frac{2 I_{DS}}{V_{GS} - V_{th}}$$

\*  $V_{DS,sat} = V_{GS} - V_{th}$  ← This is minimum  $V_{DS}$  for Nmos to operate in saturation region.

$$= \sqrt{\frac{2 I_D}{\mu_n C_{ox} \frac{W}{L}}}$$

$$\Rightarrow V_{GS} = V_{DS,sat} + V_{th}$$

$V_{GS}$  can go higher than  $V_{DS,sat}$  only by  $V_{th}$ .