

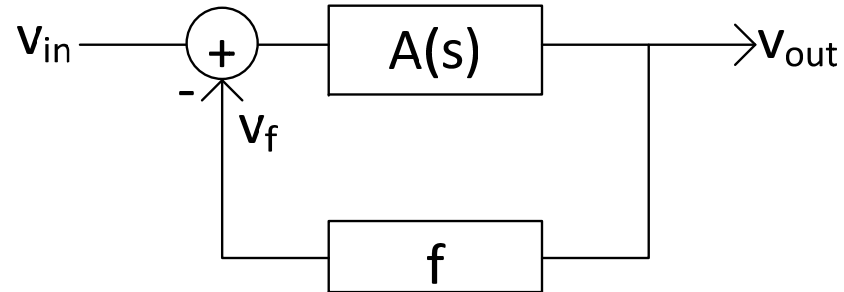
# **ECE 4220 Final Exam (Take Home)**

**Due Date: 12/17/2012, 3PM**

**Full Credit: 150-pt**

- **No collaboration**
- **No discussion with any other**
- **No software simulation**
- **Only handcalculator allowed**

# Some clarifications on feedback loop amounts



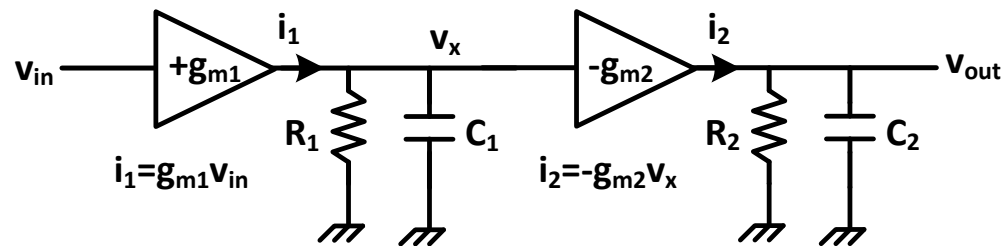
- ❑ In typical two-pole amplifier:  $A(s) = -A_o \frac{\omega_o^2}{s^2 + \frac{\omega_o}{Q}s + \omega_o^2}$ , **note:  $A_o$  is a positive number.**
- ❑ Loop gain:  $T(s) = -fA(s) = A_o \frac{\omega_o^2}{s^2 + \frac{\omega_o}{Q}s + \omega_o^2} \times f$ , **note:  $A_o \times f$  is a positive number.**
- ❑ Overall gain:  $A_f(s) = \frac{V_{out}}{V_{in}} = -A_{of} \frac{\omega_{of}^2}{s^2 + \frac{\omega_{of}}{Q_f}s + \omega_{of}^2}$ , **note:  $A_{of}$  is a positive number.**

# Problem Set-1: Feedback Amplifier Design

- Consider an open-loop 2-stage amplifier in abstract level shown below. The transconductors are ideal transconductors, i.e., input and output impedances are infinite. Each parameter is given as:

$$g_{m1} = 2 \text{ m}\Omega^{-1}, R_1 = 100 \text{ k}\Omega, C_1 = 100 \text{ fF}$$

$$g_{m2} = 4 \text{ m}\Omega^{-1}, R_2 = 10 \text{ k}\Omega, C_2 = 200 \text{ fF}.$$

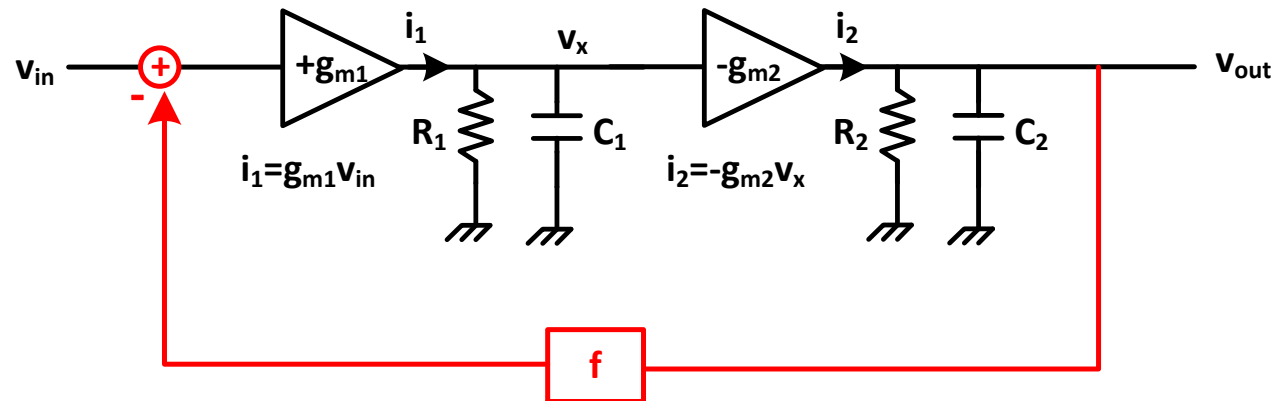


Q-1) Draw Bode plots (gain and phase plots) of transfer function,  $A(s) = \frac{V_{out}}{V_{in}}$  (5pt).

Q-2) Find the canonical form of open-loop gain,  $A(s) = -A_o \frac{\omega_o^2}{s^2 + \frac{\omega_o}{Q}s + \omega_o^2}$ . What are the system  $Q$  and the natural frequency  $\omega_o$ ? (5pt)

# Problem Set-1: Feedback Amplifier Design

□ Now let's apply a negative feedback. All the components values are the same as previous.



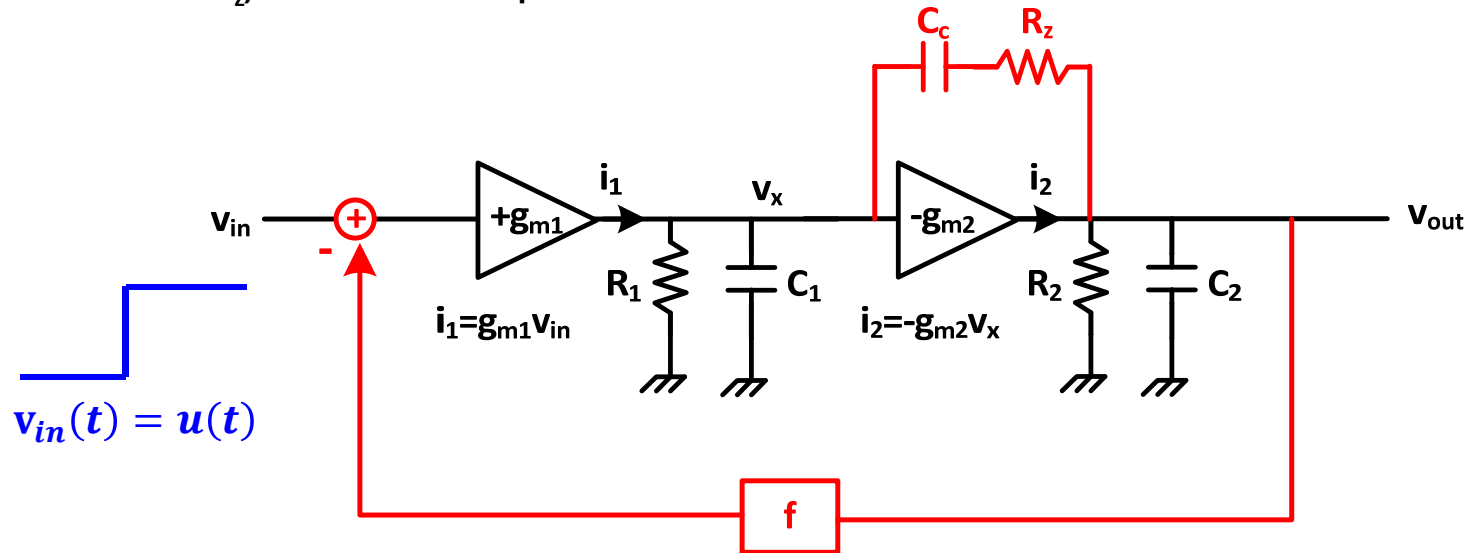
Q-3) Find the canonical form of overall closed-loop gain under the unity feedback ( $f=1$ ),  $A_f(s) = \frac{V_{out}}{V_{in}} = -A_{of} \frac{\omega_{of}^2}{s^2 + \frac{\omega_{of}}{Q_f}s + \omega_{of}^2}$ . Determine the system  $Q_f$ , peaking frequency  $\omega_{pk}$ , relative peaking magnitude of  $\left| \frac{A_f(j\omega_{pk})}{A_f(0)} \right|$ , and phase margin (PM) (20pt).

Q-4) Determine the range of feedback factor  $f$ , where phase margin (PM) is larger than  $45^\circ$  (15pt).

Q-5) Set feedback factor  $f$  to get  $PM=45^\circ$ . Determine the system  $Q_f$ , peaking frequency  $\omega_{pk}$ , and relative peaking magnitude of  $\left| \frac{A_f(j\omega_{pk})}{A_f(0)} \right|$  (10pt).

# Problem Set-1: Feedback Amplifier Design

- Apply a frequency compensation network as shown below. All the components values (except for  $C_c$  and  $R_z$ ) are the same as previous.



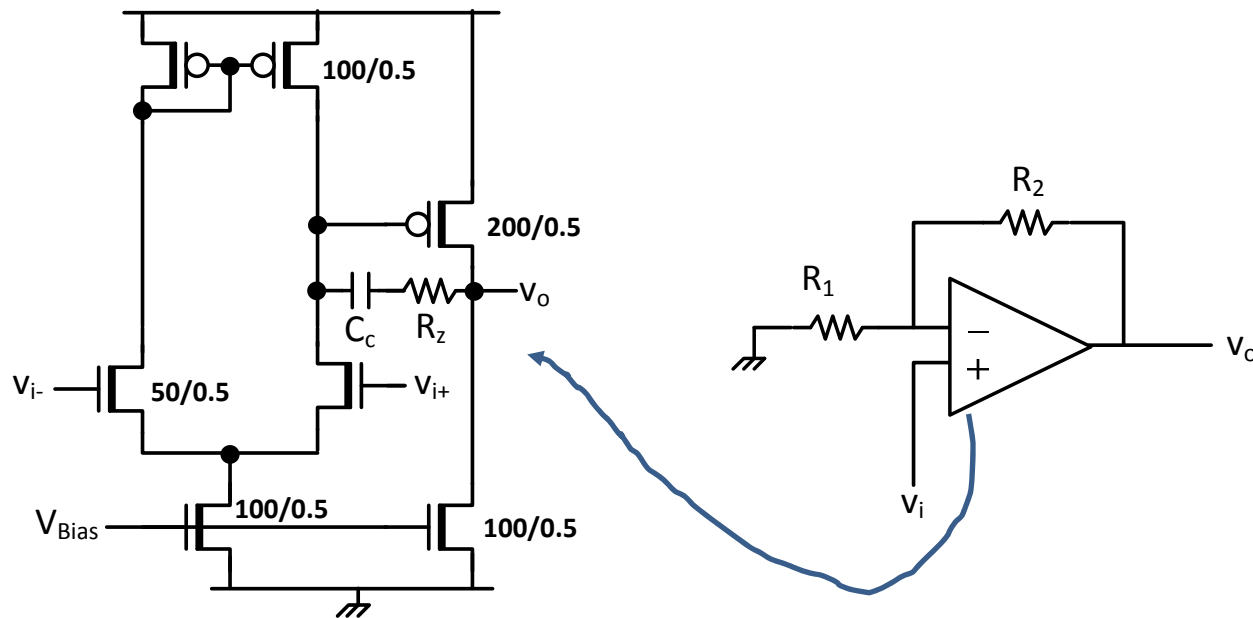
Q-6) Design the frequency compensation network  $C_c$  and  $R_z$  to meet the following conditions when unity feedback  $f=1$  (15pt):

- ①  $PM=80^\circ$ ,
- ② Overall system has only 2 poles (no zero).

Q-7) When  $f=1$  with  $PM=80^\circ$ , apply a step input  $v_{in}(t) = u(t)$ . Find output and sketch the output wave form. What is 0.1% settling time (0.1% settling time=the time when output reach 99.9% of its final value ) (10pt)?

# Problem Set-2: OP-AMP Application

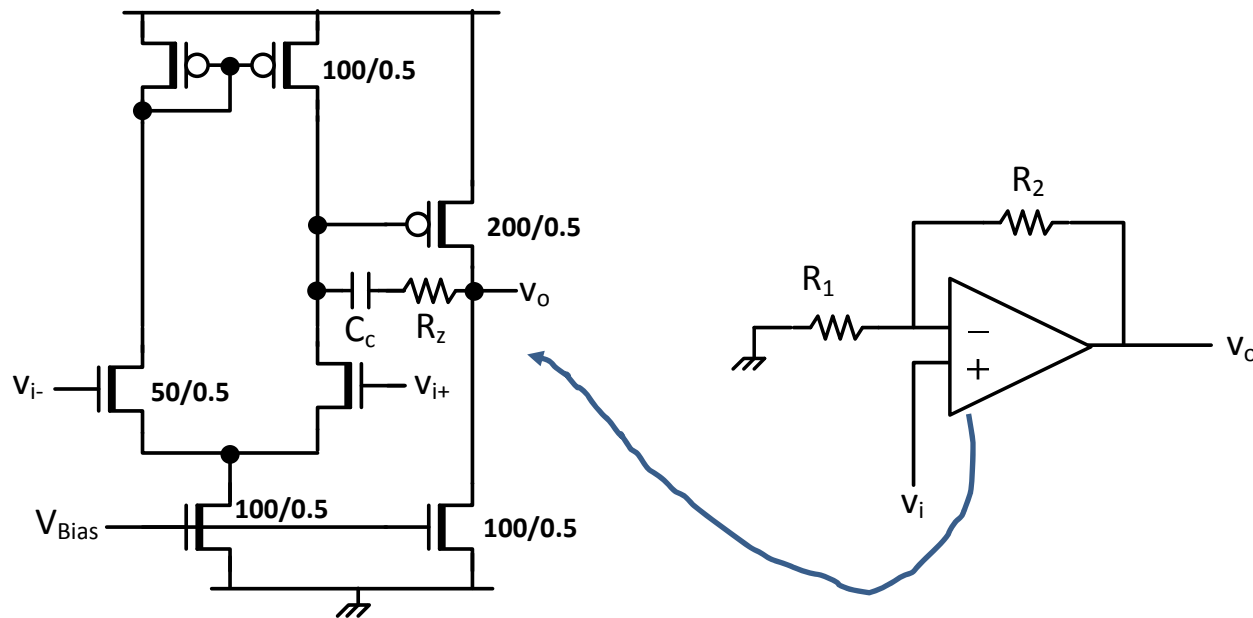
- An opamp shown below has an open-loop gain of 80dB, and it has two negative poles and one negative zero at  $\omega_{p1}=5 \times 10^3$ ,  $\omega_{p2}=10^8$ , and  $\omega_z=5 \times 10^8$  rad/s after standard miller compensation ( $C_c=30$  pF).  $\mu_n C_{ox}=150 \mu\text{A}/\text{V}^2$  and  $\mu_p C_{ox}=75 \mu\text{A}/\text{V}^2$ . Supply voltage is 3 V. A non-inverting amplifier with 20 dB of gain is configured based on the opamp.



- Q-8) Determine feedback factor ( $f$ ) and estimate BW of the non-inverting amplifier (5pt).
- Q-9) What's the phase margin of the non-inverting amplifier (10pt)?
- Q-10) What are the maximum linear input and output signal range of the non-inverting amplifier (5pt)?

# Problem Set-2: OP-AMP Application

- An opamp shown below has an open-loop gain of 80dB, and it has two negative poles and one negative zero at  $\omega_{p1}=5 \times 10^3$ ,  $\omega_{p2}=10^8$ , and  $\omega_z=5 \times 10^8$  rad/s after standard miller compensation ( $C_c=30$  pF).  $\mu_n C_{ox}=150 \mu\text{A/V}^2$  and  $\mu_p C_{ox}=75 \mu\text{A/V}^2$ . Supply voltage is 3 V. A non-inverting amplifier with 20 dB of gain is configured based on the opamp.



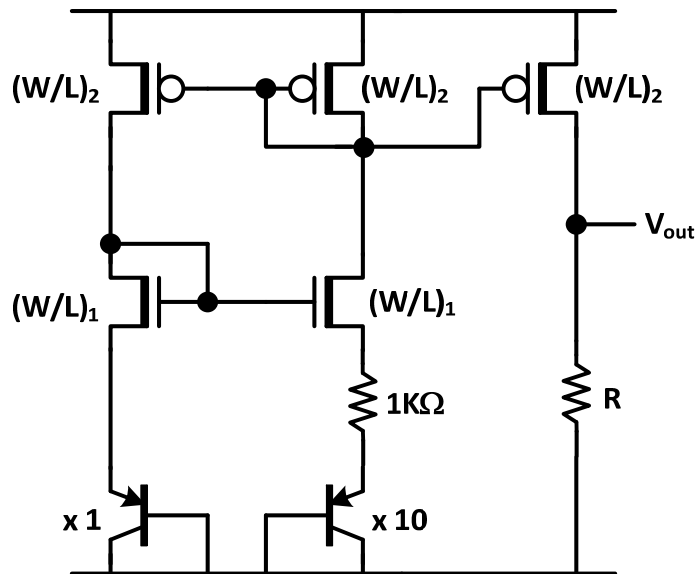
Q-11) Assume that you apply the maximum sinusoidal input to the non-inverting amplifier. Now you increase the input frequency. What's the maximum input frequency at which the output is not distorted due to slew-rate limitation (10pt)?

Q-12) If you change the feedback factor so that the non-inverting amplifier has 10 dB gain while using the same op amp, then what are the BW and phase margin of the non-inverting amplifier (5pt)?

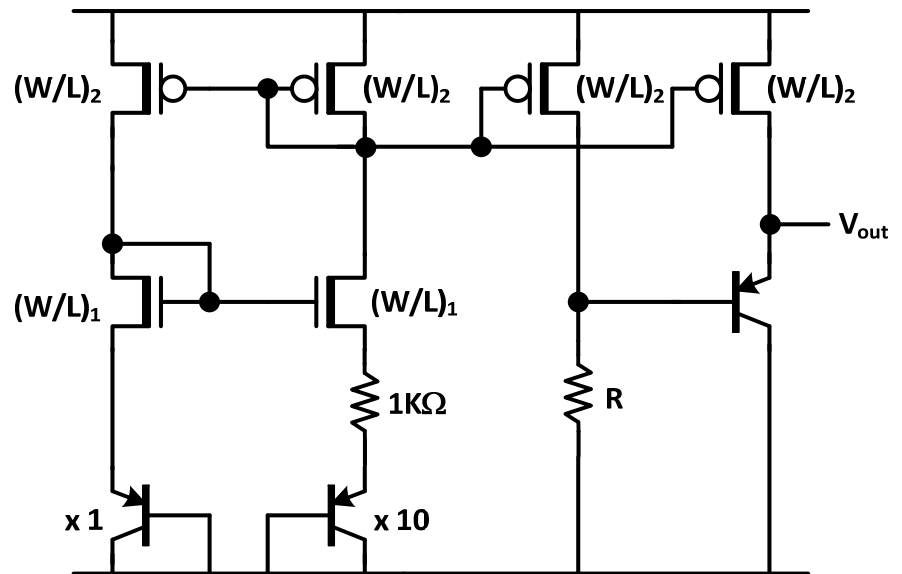
# Problem Set-3: PTAT & Bandgap Reference

- Use these parameters for the question in this part:  $V_T = KT/q = 26 \text{ mV}$  at  $300^\circ\text{K}$ ,  $|V_{be}| = 0.7 \text{ V}$ ,  
 $\frac{\partial |V_{be}|}{\partial T} = -1.65 \text{ mV}/^\circ\text{C}$ .

<Electronic Thermometer>



<Bandgap Reference>



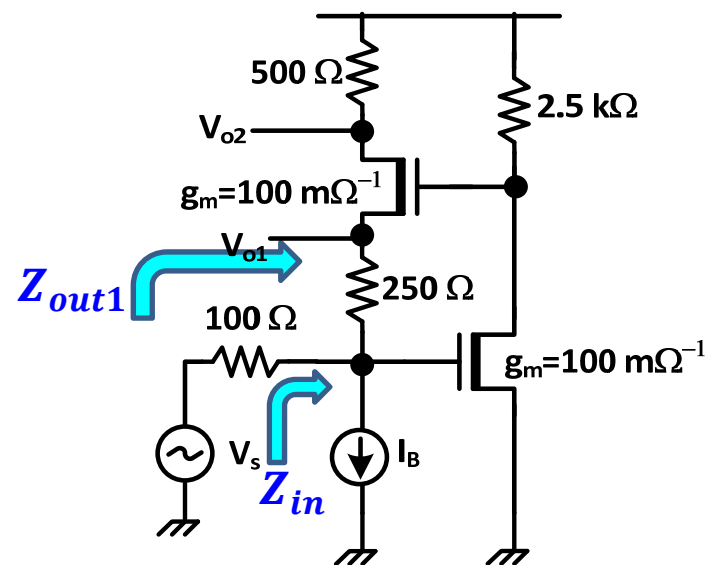
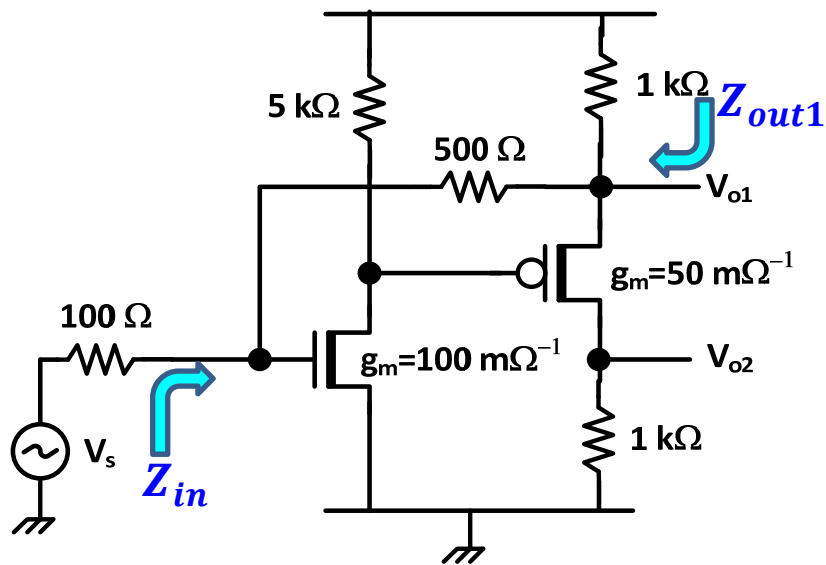
Q-13) In the electronic thermometer, let's assume all PMOS and NMOS have no effect of channel length modulation. Set R value so that we can read the absolute temperature T as  $V_{out} = T/1000$ . For example,  $V_{out} = 0.3\text{V}$  at  $300^\circ\text{K}$ , and  $V_{out} = 0.4\text{V}$  at  $400^\circ\text{K}$  (10pt).

Q-14) In the Bandgap reference, determine R so that  $V_{out}$  is insensitive to temperature variation at  $300^\circ\text{K}$  (5pt).



# Problem Set-4: Shunt Feedback Amplifiers

□ Assume output impedance ( $r_o$ ) of NMOS and PMOS is infinite.



Q-15) For the left side amplifier, Find loop gain ( $T$ ), input impedance ( $Z_{in}$ ), output impedance ( $Z_{out1}$ ), voltage gains  $\frac{V_{o1}}{V_s}$  and  $\frac{V_{o2}}{V_s}$  (10pt).

Q-16) For the right side amplifier, Find loop gain ( $T$ ), input impedance ( $Z_{in}$ ), output impedance ( $Z_{out1}$ ), voltage gains  $\frac{V_{o1}}{V_s}$  and  $\frac{V_{o2}}{V_s}$  (10pt).