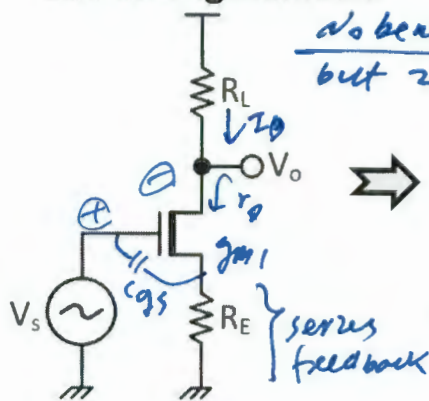


# Source Coupling

❑ What's the benefit of differential topology?

Source Degeneration



series feedback

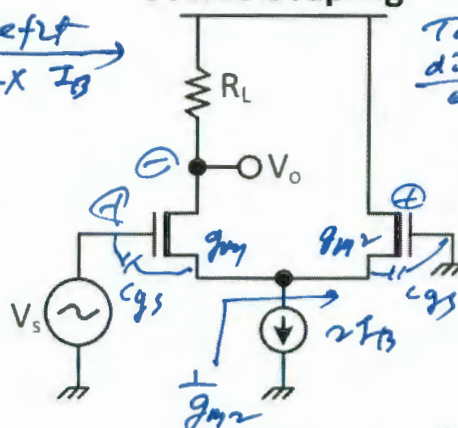
loop gain  $\rightarrow T = g_{m1} R_E$

$$A_v = \frac{g_{m1} R_L}{1 + g_{m1} R_E}$$

$$C_{gs} \rightarrow \frac{C_{gs}}{1 + g_{m1} R_E}$$

$$r_o \rightarrow r_o (1 + g_{m1} R_E)$$

Source Coupling



series feedback

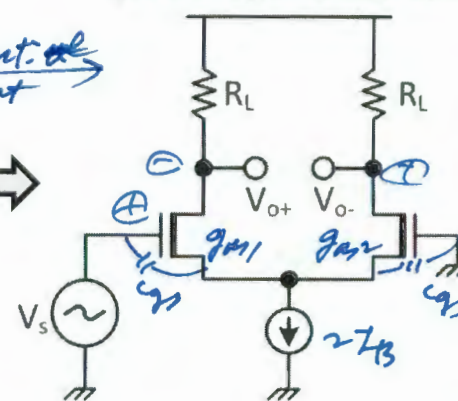
$$T = g_{m1} \cdot \frac{1}{g_{m2}}$$

$$A_v = \frac{g_{m1} R_L}{1 + g_{m1} \frac{1}{g_{m2}}}$$

$$C_{gs} \rightarrow \frac{C_{gs}}{1 + g_{m1} \frac{1}{g_{m2}}}$$

$$r_o \rightarrow r_o (1 + g_{m1} \frac{1}{g_{m2}})$$

Differential Topology  
(with single-ended driving)



series feedback

$$T = g_{m1} \cdot \frac{1}{g_{m2}}$$

$$A_v = \frac{g_{m1} R_L}{1 + g_{m1} \frac{1}{g_{m2}}} \times 2$$

$$C_{gs} \rightarrow \frac{C_{gs}}{1 + g_{m1} \frac{1}{g_{m2}}}$$

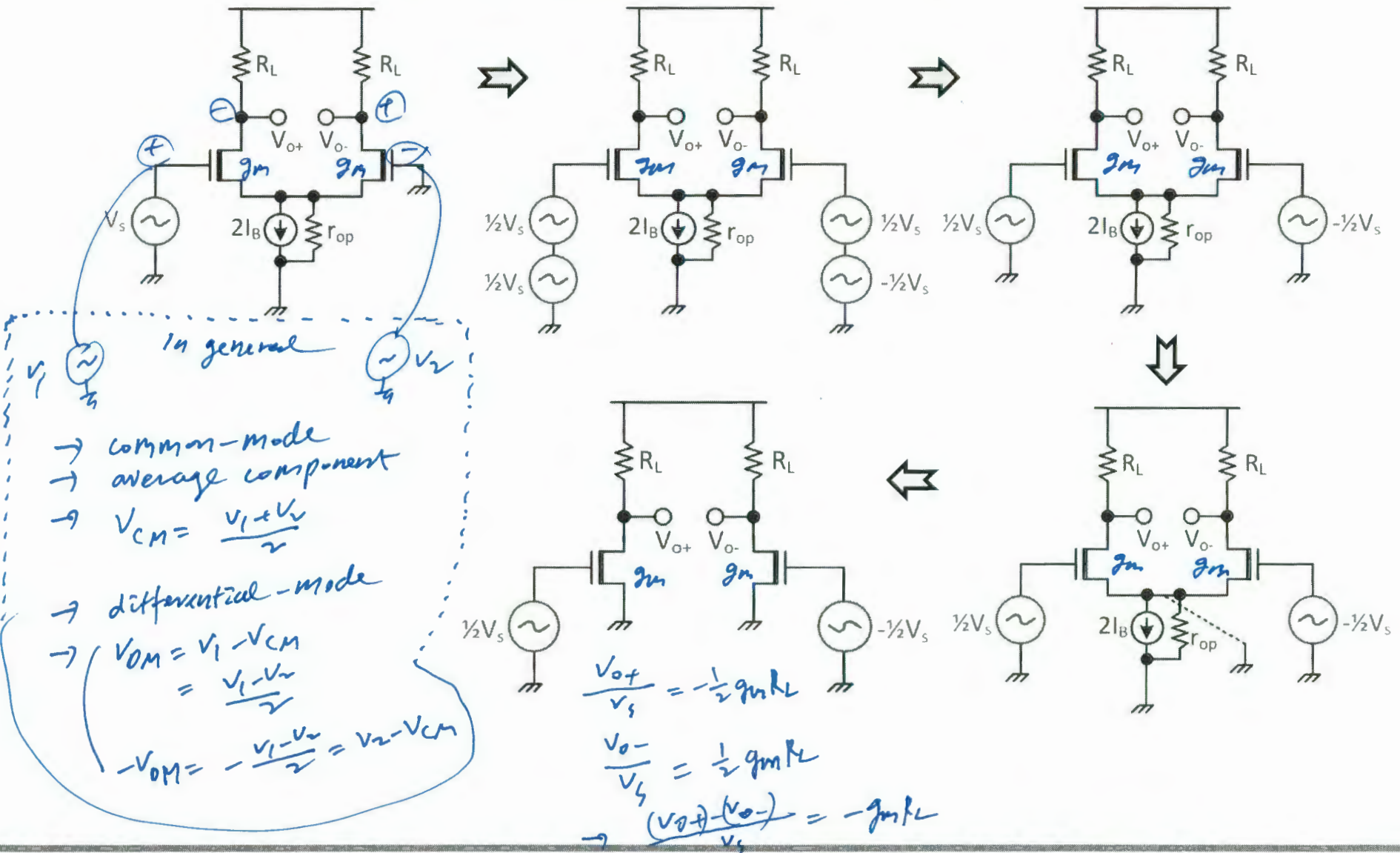
$$r_o \rightarrow r_o (1 + g_{m1} \frac{1}{g_{m2}}) \times \frac{1}{2}$$

Single-ended  
output impedance

differential  
output impedance

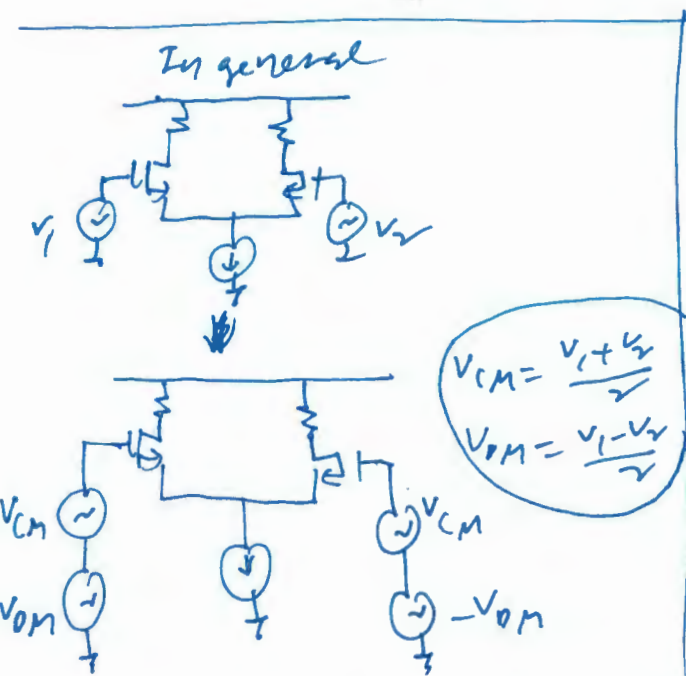
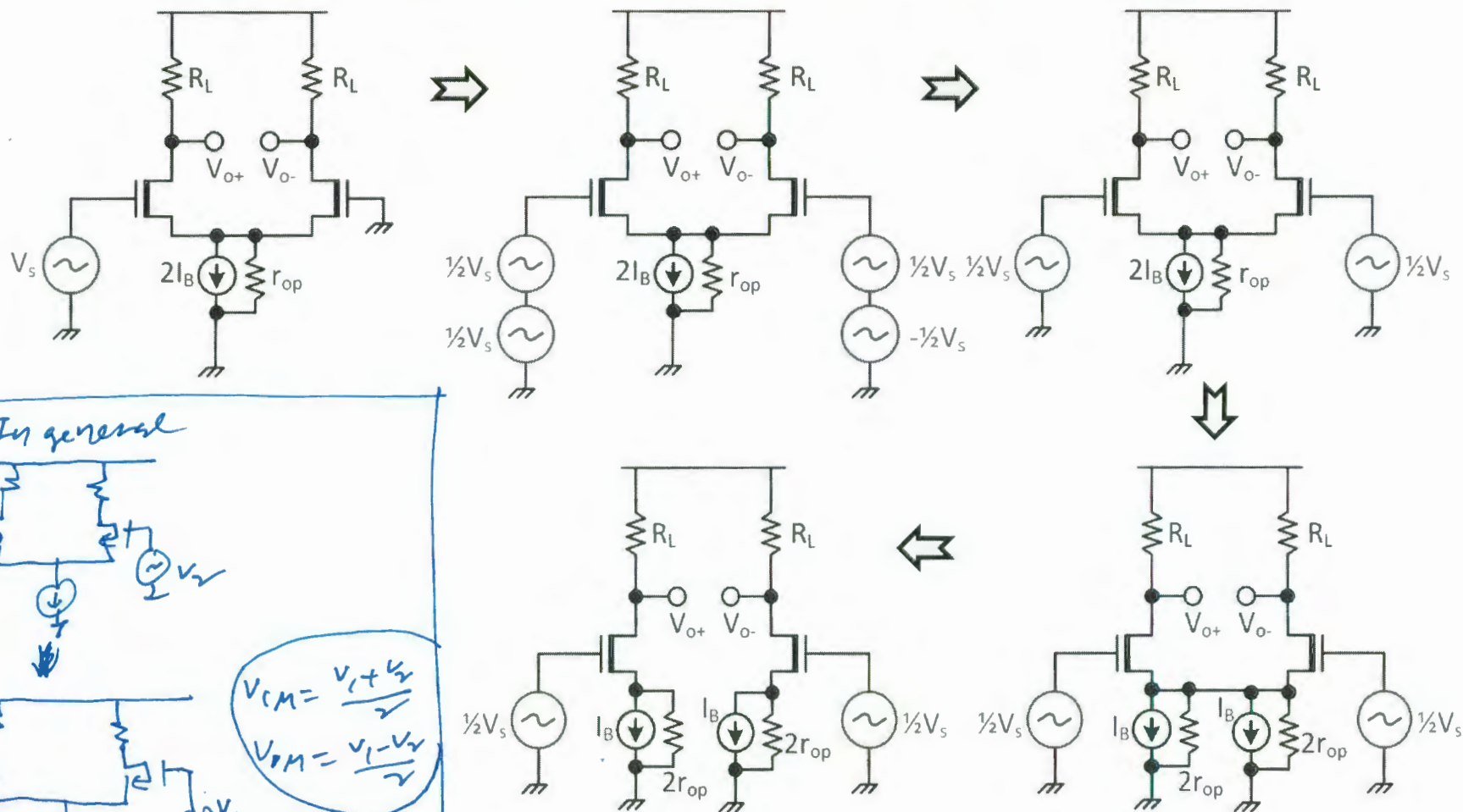
# Single-Ended vs. Differential Driving

□ Topological equivalence in terms of differential-mode driving



# Single-Ended vs. Differential Driving

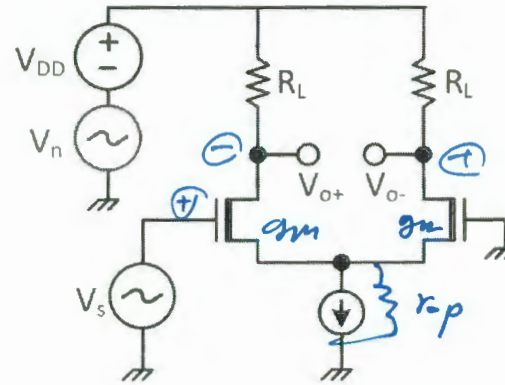
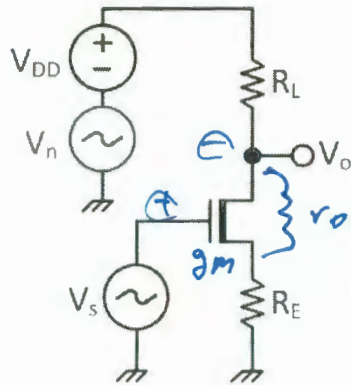
□ Topological equivalence in terms of common-mode driving





# Power Supply Noise Rejection

□ What's the benefit of differential topology?



$$A_{Vs} = \frac{v_o}{v_s} = -\frac{g_m R_L}{1 + g_m R_E}$$

$$A_{Vn} = \frac{v_o}{V_n} = \frac{r_o(1 + g_m R_E)}{R_L + r_o(1 + g_m R_E)} \approx 1$$

⊛ power supply rejection ratio (PSRR)

$$= \left| \frac{A_{Vs}}{A_{Vn}} \right| = \frac{g_m R_L}{1 + g_m R_E}$$

$$A_{Vs} = \frac{v_o}{v_s} = \frac{v_{o+} - v_{o-}}{v_s} = -g_m R_L$$

$$\Rightarrow \frac{v_{o+}}{v_s} = -\frac{1}{2} g_m R_L$$

$$\Rightarrow \frac{v_{o-}}{v_s} = \frac{1}{2} g_m R_L$$

$A_{Vn} = 0 \rightarrow V_n \Rightarrow$  common-mode signal

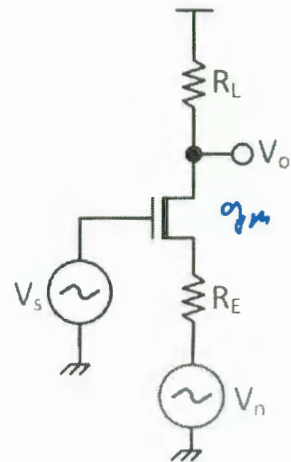
$$\frac{v_{o+}}{V_n} = \frac{r_o(1 + 2g_m r_{op})}{R_L + r_o(1 + 2g_m r_{op})}$$

$$\frac{v_{o-}}{V_n} = \frac{r_o(1 + 2g_m r_{op})}{R_L + r_o(1 + 2g_m r_{op})}$$

$$\Rightarrow \text{PSRR} = \infty$$

# Ground Noise Rejection

□ What's the benefit of differential topology?

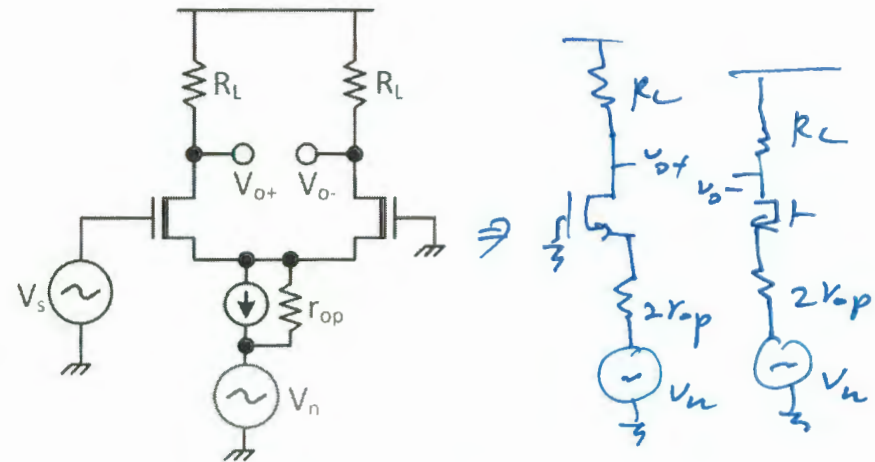


$$A_{v_s} = \frac{V_o}{V_s} = -\frac{g_m R_L}{1 + g_m R_E}$$

$$A_{v_n} = \frac{V_o}{V_n} = \frac{g_m R_L}{1 + g_m R_E}$$

⊗ Ground supply rejection ratio (GSR)

$$= \left| \frac{A_{v_s}}{A_{v_n}} \right| = 1$$



$$\begin{aligned} \frac{V_{o+}}{V_n} &= \frac{g_m R_L}{1 + 2g_m r_{op}} \\ \frac{V_{o-}}{V_n} &= \frac{g_m R_L}{1 + 2g_m r_{op}} \end{aligned}$$

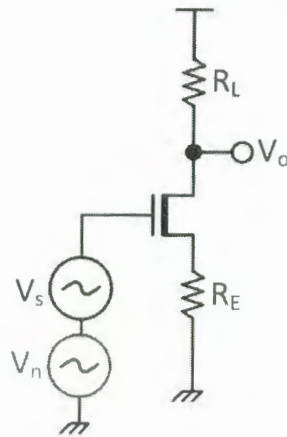
$$\rightarrow \frac{V_{o+} - V_{o-}}{V_n} = 0$$

→  $V_n \Rightarrow$  common-mode signal

$$\rightarrow GSR = \infty$$

# Common-Mode Noise Rejection

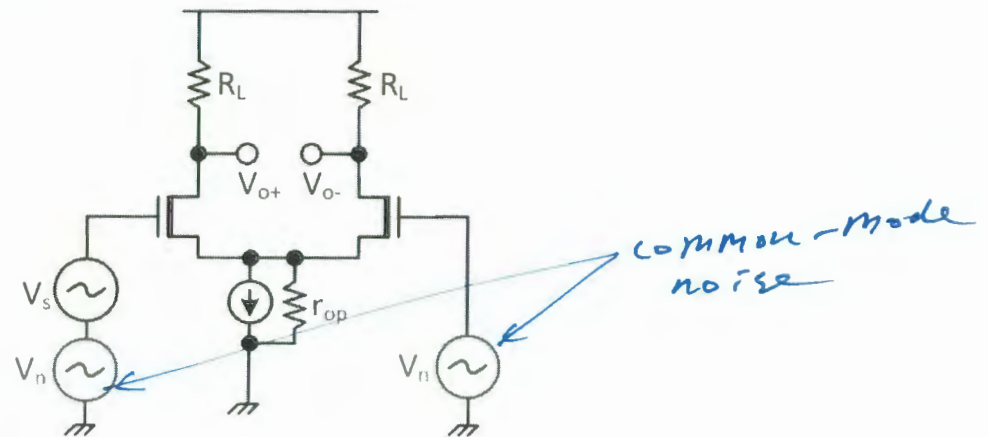
□ What's the benefit of differential topology ?



$$A_{V_S} = \frac{V_o}{V_S} = -\frac{g_m R_L}{1 + g_m R_E}$$

$$A_{V_N} = \frac{V_o}{V_N} = -\frac{g_m R_L}{1 + g_m R_E}$$

CMRR  $\propto g_m R_{op}$



$$A_{V_S} = \frac{V_o}{V_S} = \frac{V_{o+} - V_{o-}}{V_S} = -g_m R_L$$

$$A_{V_N} = 0$$

$$\rightarrow \frac{V_{o+}}{V_N} = \frac{-g_m R_L}{1 + 2g_m R_{op}}$$

$$\frac{V_{o-}}{V_N} = \frac{-g_m R_L}{1 + 2g_m R_{op}}$$

$\rightarrow$  (\*) common-mode rejection ratio

$$= \frac{\text{differential gain}}{\text{single-ended gain of common-mode signal}} = \frac{g_m R_L}{\frac{g_m R_L}{1 + 2g_m R_{op}}}$$

$$= 1 + 2g_m R_{op} \approx 2g_m R_{op}$$

# DC Stability (1)

□ What if NMOS and PMOS bias currents are not matched?

