

CMOS RF Noise, Scaling, and Compact Modeling for RFIC Design

Angelos Antonopoulos, Matthias Bucher, Konstantinos Papathanasiou, Nikolaos Makris,
Rupendra K. Sharma, Paulius Sakalas^{1,2}, and Michael Schroter¹

Dept. of Electronic and Computer Engineering, Technical University of Crete, 73100 Chania, Greece

¹Dept. of Electrical and Computer Engineering, TU Dresden, 01062 Dresden, Germany

²Semiconductor Physics Institute, CPST, 01108 Vilnius, Lithuania

Abstract — This work presents an analysis of high frequency noise and linearity performance of a 90 nm CMOS process. Measurements are performed for a wide range of nominal gate lengths and bias points at high frequency. Modeling is based on the EKV3 compact model in Spectre RF circuit simulator from Cadence. The model shows correct scalability for noise and linearity accounting for short channel effects (SCEs), such as velocity saturation (VS) and channel length modulation (CLM). Results are presented versus a common measure of channel inversion level, named inversion coefficient. Optimum performance is shown to gradually shift from higher to lower levels of moderate inversion, when scaling from 240 nm to 100 nm. The same trend is observed from investigating the transconductance frequency product (TFP) of a common-source (CS) LNA for technology nodes ranging from 180 nm to 22 nm.

Index Terms — Compact model, distortion analysis, dynamic range, high frequency noise, metal oxide semiconductor field effect transistor (MOSFET), minimum noise figure (NF_{min}), moderate inversion.

I. INTRODUCTION

Scaling CMOS to the deca-nanometer regime, a tremendous improvement of RF performance has been reported in terms of conventional figures of merit (FoM), such as f_T and f_{max} [1]-[2]. However, a large amount of industrial IC design of RF front ends is still done using CMOS technology nodes such as 180 nm and 90 nm, due to their high RF-performance-to-cost ratio [3]. Therefore, accurate modeling of these CMOS processes remains of high interest. Previous published work has shown RF noise performance and harmonic distortion for specific bias points and limited frequency range [4]-[6]. In this paper, we expand the work of previous publications presenting a detailed investigation of RF noise and harmonic distortion expressed by NF_{min} and 3rd-order intercept points (P_{IP3} and V_{IP3}), respectively, based on measurements over a wide range of frequency, bias points and nominal gate lengths. These FoMs, which determine the dynamic range of a circuit, are shown with respect to nominal gate length and inversion level, experiencing a shift in their optimum performance to lower inversion level when scaling from 240 nm down to 100 nm. The EKV3 compact model efficiently describes this behavior.

II. RF NOISE

A. Noise Measurements

Noise measurements have been performed using a system setup consisting of a vector network analyzer, tuners, filters and a spectrum analyzer with a noise figure measurement personality. MOS devices of channel width $W=40 \times 2$ μm and nominal gate length ranging from $L=240$ nm to $L=100$ nm have been measured up to 20 GHz. The drain-source voltage (V_{DS}) is kept constant at 1.2 V whereas the gate-source voltage (V_{GS}) is swept from 0 to 1 V. Noise parameters NF_{min}, R_n , and Γ_{opt} are expressed in terms of two-port network theory as:

$$NF = NF_{min} + \frac{R_n}{G_s} |Y_s - Y_{opt}|^2. \quad (1)$$

G_s is the source conductance and Y_s the source admittance. Optimum admittance results from the measured optimum source reflection coefficient Γ_{opt} via

$$Y_{opt} = Y_0 \frac{(1 - \Gamma_{opt})}{(1 + \Gamma_{opt})}. \quad (2)$$

Y_0 is typically equal to 0.02 S. Measured noise parameters along with EKV3 model results (symbols and lines, respectively, as also throughout the rest of the text) are plotted in Fig. 1, up to 20 GHz for an NMOS device of $L=100$ nm, operating in saturation.

B. R_n , Γ_{opt} and NF_{min} with Scaling and Inversion Level

To investigate the behavior of NF_{min} with inversion level we use the inversion coefficient, IC introduced in [7], [8], which is given by simply normalizing drain current I_D to a specific current I_{spec} , as $IC = I_D/I_{spec}$. The latter is given by (3) and depends on the effective mobility μ_{eff} and slope factor n , while I_0 is called the technology current [9]. U_T is the thermal voltage.

$$I_{spec} = 2nU_T^2 \mu_{eff} C_{ox} \frac{W_{eff}}{L_{eff}} = I_0 \cdot \frac{W_{eff}}{L_{eff}} \quad (3)$$

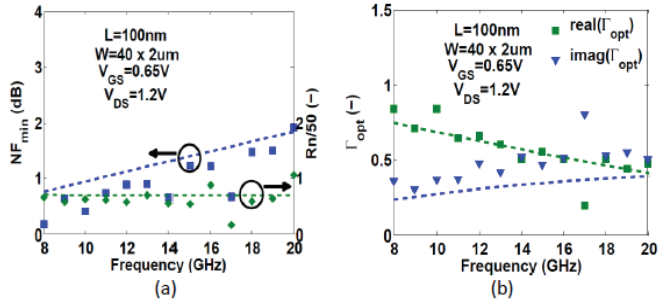


Fig. 1. (a) NF_{min} and $R_n/50$, (b) real and imaginary part of Γ_{opt} vs. frequency.

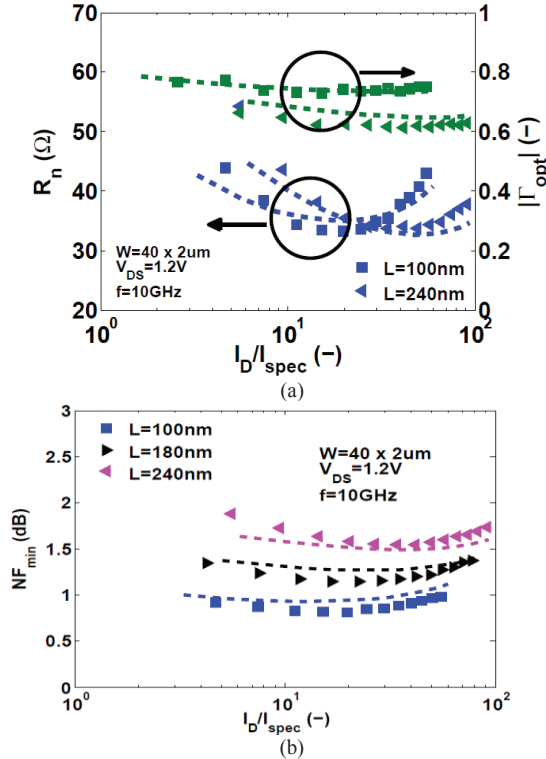


Fig. 2. (a) R_n and $|\Gamma_{opt}|$, and (b) NF_{min} vs. IC for NMOS devices of L values ranging from 240 nm to 100 nm.

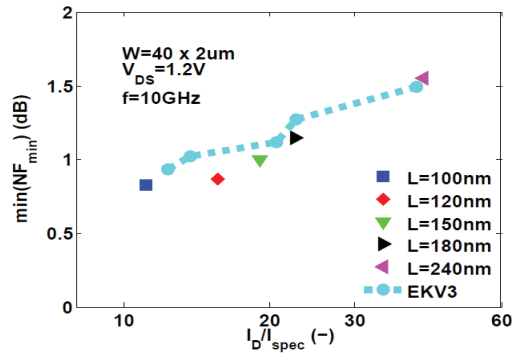


Fig. 3. Minimum values of NF_{min} vs. IC for NMOS devices of different L.

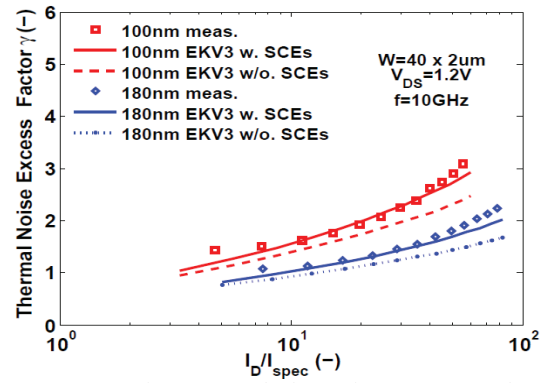


Fig. 4. γ vs. IC for NMOS devices of L=100 nm and L=180 nm, with and without accounting for SCEs.

For $IC < 0.1$ the device is in weak inversion (W.I.). Moderate inversion (M.I.) corresponds to $0.1 < IC < 10$, whereas IC values greater than 10, denote strong inversion (S.I.) operation. I_o amounts to 740 nA for the present NMOS devices.

Equivalent noise resistance, R_n and magnitude of optimum source reflection coefficient, $|\Gamma_{opt}|$, are presented in Fig. 2 (a) with respect to IC for NMOS devices of L=100 nm and L=240nm. NF_{min} is also plotted in Fig. 2 (b) versus IC for different nominal gate length NMOS devices operating in saturation at 10 GHz. The results are in line with those presented in [10]. It is obvious that as we scale down to 100 nm, NF_{min} as well as R_n minima move from higher to lower IC values. This is more evident in Fig. 3, where the minimum values of NF_{min} are presented with respect to IC, for NMOS devices of nominal gate length ranging from 240 nm to 100 nm. It should be underlined that for L=100 nm, the minimum NF_{min} value (0.82 dB) appears at the vicinity of M.I. to S.I., and specifically at $IC=11$.

C. Thermal Noise Excess Factor

Noise in MOSFETs is dominated by the channel thermal noise given by (4), which is described by its power spectral density (S_{id}).

$$S_{id} = 4kT \frac{I_{spec}}{U_T} g_n \quad (4)$$

Thermal noise is characterized by the thermal noise excess factor γ and the thermal noise parameter δ , introduced by Van der Ziel [11]. Both are presented in (5) with G_n representing the thermal noise conductance (g_n is its normalized value).

$$\delta = \frac{G_n}{G_{dso}}, \quad \gamma = \frac{G_n}{G_m} \quad (5)$$

δ is evaluated for zero V_{DS} , thus it has no specific meaning in terms of RFIC design.

On the other hand, the thermal noise excess factor γ , which represents the noise that is generated at the drain of a transistor, for a given gate transconductance, is of major importance since it is derived at any given operating point. The short-channel effects on thermal noise, such as CLM, VS and carrier heating, affect mobility and hence G_m , effective length, and γ [9]. γ is used for determining the noise figure of a common-source LNA [12]. Fig. 4 presents the thermal noise excess factor, with respect to IC, with and without accounting for SCEs. It is clear that γ is greatly underestimated when SCEs are neglected in noise calculations, especially for the shorter gate length device of $L=100$ nm and for operation in S.I.

III. HIGH FREQUENCY DISTORTION ANALYSIS

Distortion analysis in MOSFETs is usually expressed by the 3rd order products generated by the MOSFETs nonlinearities expressed in terms of 3rd order intermodulation input intercept points P_{IP3} and V_{IP3} . The nonlinearities mainly arise from harmonics [13]-[15] induced by higher order derivatives of the channel current I_D with respect to V_{GS} , especially by the 3rd order derivative G_{m3} , calculated via (6).

$$G_m = \frac{\partial I_D}{\partial V_{GS}}, G_{m2} = \frac{\partial^2 I_D}{\partial V_{GS}^2}, G_{m3} = \frac{\partial^3 I_D}{\partial V_{GS}^3} \quad (6)$$

In general, linearity FoMs are exported from DC measurements. However it is also useful to study these metrics at high frequency, since this would be more meaningful in terms of RFIC design. Therefore RF measurements were performed for several V_{DS} and V_{GS} values and linearity metrics were extracted at 1.1 GHz. G_m , G_{m2} and G_{m3} measurements as well as EKV3 simulation data are shown in Fig. 5 versus IC for the shorter device of $L=100$ nm biased in saturation. P_{IP3} and V_{IP3} are calculated through (7) and presented in Fig. 6 (a) and Fig. 6 (b), respectively, for the longest and shortest measured devices. R_S is a matched input resistance equal to 50 Ω . The model results are in close proximity with measurements and recent published work [10], [14], [15].

Since for low distortion operation all linearity FoMs should be as high as possible, it is worth noticing that moving towards shorter length devices, the peak value of linearity metrics is moving to lower inversion levels, experiencing the same shift as NF_{min} , which for $L=100$ nm approaches the center of M.I. region ($IC=1$).

$$P_{IP3} = \left| \frac{2G_m}{3G_{m3}R_S} \right|, V_{IP3} = \sqrt{\frac{24G_m}{G_{m3}}} \quad (7)$$

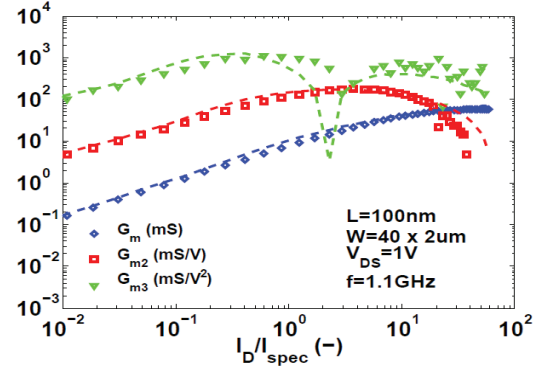


Fig. 5. G_m , G_{m2} and G_{m3} vs. IC.

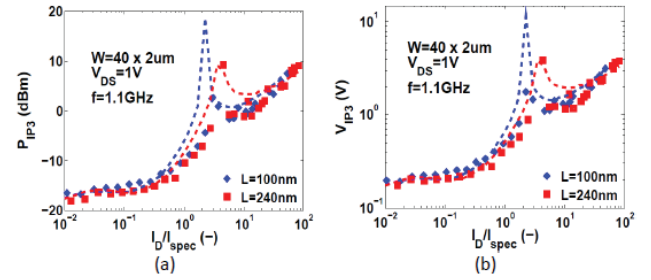


Fig. 6. (a) P_{IP3} , and (b) V_{IP3} vs. IC for NMOS devices of $L=100$ nm and $L=240$ nm.

IV. FIGURE OF MERIT FOR CS LNA

For characterizing a low-power LNA performance, an overall FoM is usually used, given by (8) [16]:

$$FoM_{LPLNA} = \frac{G_v f_{RF}}{(F-1)P_{cons}} \propto \frac{G_m f_T}{I_D} = TFP \quad (8)$$

G_v is the voltage gain, f_{RF} is the frequency of operation, F stands for the noise factor and P_{cons} is the power consumption.

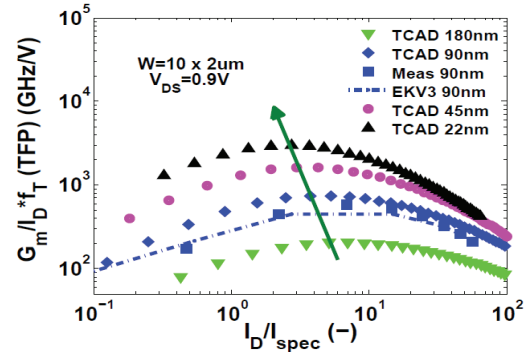


Fig. 7. TFP vs. IC for NMOS devices of L values ranging from 180 nm to 22 nm.

Recently, Taris et al. [16] showed that this low-power LNA FoM is proportional to TFP, when a CS topology is

considered. Moreover TFP becomes maximum in M.I. as shown in [17], [18] for 180 nm and 130 nm CMOS technologies, respectively. Therefore, it is meaningful to study its behavior with technology scaling. In Fig. 7, TFP for measured data, EKV3 model and TCAD simulations from 180 nm to 22 nm technology nodes, is plotted versus IC. It is evident that not only TFP improves with technology scaling, but also its peak value is shifted from higher to lower IC values, close to the center of M.I., when scaling down to 22 nm.

V. CONCLUSIONS

In this work, we outline the relation between inversion coefficient, nominal gate length and FoMs essential for RFIC design, such as NF_{min} , P_{IP3} and V_{IP3} . For this purpose RF and RF noise measurements of a 90 nm CMOS process were performed for a wide range of devices, bias points and frequencies. The inversion coefficient is used to indicate the shift of optimum performance close to or within the moderate inversion region. Moreover RF performance of a CS LNA topology, expressed in terms of TFP, is studied. Best performance is achieved close to the center of M.I. as technology scales down from 180 nm to 22 nm. Hence it is expected that approaching the sub-30 nm CMOS regime the existing trade-off among power consumption, noise and linearity will become more relaxed in the M.I. region.

ACKNOWLEDGEMENT

We acknowledge the partial financial support of the "NexGenMiliWave" project (MIKPO2-ΣE-B/E-II), co-financed by the European Regional Development Fund (ERDF) and Greek national funds, under the "Hellenic Technology Clusters in Microelectronics – Phase 2" program, and of the Heracleitus II program co-financed by the European Social Fund (ESF) and Greek national funds, through the operational program "Education and Lifelong Learning", within the National Strategic Reference Framework (NSRF).

REFERENCES

- [1] S.-C. Wang, P. Su, K.-M. Chen, K.-H. Liao, B.-Y. Chen, S.-Y. Huang, C.-C. Hung, G.-W. Huang, "Comprehensive Noise Characterization and Modeling for 65-nm MOSFETs for Millimeter-Wave Applications", *IEEE Trans. Microwave Theory Techn.*, vol. 58, no. 4, pp. 740-746, Apr. 2010.
- [2] L. Poulain, N. Waldhoff, D. Gloria, F. Danneville, G. Dambrine, "Small signal and HF noise performance of 45 nm CMOS technology in mmW range", *IEEE Radio Frequency Integrated Circuits Symp.*, pp. 1-4, June 2011.
- [3] Europractice, Activity Report 2011, Europractice IC Service.
- [4] J.-C. Guo, Y.-M. Lin, "A Compact RF CMOS Modeling for Accurate High-Frequency Noise-Simulation in Sub-100-nm MOSFETs", *IEEE Trans. Computer-Aided Design Integr. Circuits Syst.*, vol. 27, no. 9, pp. 1684-1688, Sept. 2008.
- [5] A. F. Tong, W. M. Lim, K. S. Yeo, C. B. Sia, W. C. Zhou, "A Scalable RFCMOS Noise Model", *IEEE Trans. Microwave Theory Tech.*, vol. 57, no. 5, pp. 1009-1019, May 2009.
- [6] V. M. Mahajan, P. R. Patalay, R. P. Jindal, H. Shichijo, S. Martin, F.-C. Hou, C. Machala, D. E. Trombley, "A Physical Understanding of RF Noise in Bulk nMOSFETs With Channel Lengths in the Nanometer Regime", *IEEE Trans. Electron Devices*, vol. 59, no. 1, pp. 197-205, Jan. 2012.
- [7] M. Bucher, C. Lallement, C. Enz, "An Efficient Parameter Extraction Methodology for the EKV MOSFET Model", *IEEE Int. Conf. Microelectronic Test Struct.*, vol. 9, pp. 145-150, 1996.
- [8] A. Bazigos, M. Bucher, F. Krummenacher, J.-M. Sallese, A. Roy, C. Enz, "EKV3 MOSFET Compact Model Documentation Model Version 301.02", Technical University of Crete, July 2008.
- [9] C. Enz, E. Vittoz, "Charge Based MOS Transistor Modeling", John Wiley and Sons, Chichester, 2006.
- [10] P. H. Woerlee, M. J. Knitel, R. van Langevelde, D. B. M. Klaassen, L. F. Tiemeijer, A. J. Scholten, A. T. A. Zegers-van Duijnhoven, "RF-CMOS performance trends", *IEEE Trans. Electron Devices*, vol. 48, no. 8, pp. 1776-1782, Aug. 2001.
- [11] A. van der Ziel, Noise in Solid State Devices and Circuits. New York: Wiley, 1986.
- [12] C. Enz, "MOS Transistor Modeling for RF IC Design", MEAD Education, Lausanne, 2010.
- [13] T. Soorapanth, T. H. Lee, "RF Linearity of Short-Channel MOSFETs", *1st Int. Workshop on Design of Mixed-Mode Integrated Circuits and Applications*, pp. 81-84, July 1997.
- [14] R. van Langevelde, L. F. Tiemeijer, R. J. Havens, M. J. Knitel, R. F. M. Roes, P. H. Woerlee, D. B. M. Klaassen, "RF-Distortion in Deep-Submicron CMOS Technologies", *Int. Electron Devices Meeting*, pp. 807-810, 2000.
- [15] I. Kwon, K. Lee, "An Accurate Behavioral Model for RF MOSFET Linearity Analysis", *IEEE Microwave and Wireless Components Letters*, vol. 17, no. 12, pp. 897-899, Dec. 2007.
- [16] T. Taris, H. Kraimia, J.B. Begueret, Y. Deval, "MOSFET Modeling for Ultra Low-Power RF Design", nano-tera.ch, EPFL, 2011.
- [17] A. Shameli, P. Heydari, "Ultra-low power RFIC design using moderately inverted MOSFETs: an analytical/experimental study", *IEEE Radio Frequency Integrated Circuits Symp.*, pp. 470-473, June 2006.
- [18] A. Mangla, C. Enz, J.-M. Sallese, "Figure-of-merit for optimizing the current-efficiency of low-power RF circuits", *18th Int. Conf. Mixed Design of Int. Circ. Syst. (MIXDES)*, pp. 85-89, June 2011.