



(3)

(3) Noise power at input is

$$P_{N, in} = K T \Delta f \quad (\text{Because attenuator is matched to source})$$

From (2)

$$P_{N, out} = \frac{1}{R_o} \left\{ \frac{V_s^2}{4} \frac{(R_o - R_x)^2}{(R_o + R_x)^2} + \frac{V_{N_1}^2}{4} \frac{(R_o - R_x)^2}{(R_o + R_x)^2} + \frac{V_{N_2}^2}{4} + \frac{V_y^2}{4} \frac{R_o^2}{\left(\frac{R_o + R_x + R_y}{2}\right)^2} \right\}$$

$$= \frac{1}{R_o} \left\{ K T \Delta f \frac{(R_o - R_x)^2}{(R_o + R_x)^2} + K T \Delta f R_x + K T \Delta f R_y \frac{R_o^2}{\left(\frac{R_o + R_x + R_y}{2}\right)^2} \right\}$$

$$\Rightarrow P_{N, out} = \frac{K T \Delta f}{R_o} \left[ \frac{(R_o - R_x)^2}{R_o + R_x} + R_x + \frac{R_y R_o^2}{\left(\frac{R_o + R_x + R_y}{2}\right)^2} \right]$$

$$\text{From } R_o = R_x + \frac{R_y (R_x + R_o)}{R_y + R_x + R_o} \Rightarrow R_o = R_x \sqrt{1 + \frac{2 R_y}{R_x}}$$

$$\text{Let } R_z = \sqrt{1 + \frac{2 R_y}{R_x}} \Rightarrow R_o = R_z R_o$$

$$\Rightarrow \left[ \frac{(R_o - R_x)^2}{R_o + R_x} + R_x + \frac{4 R_y R_o^2}{(R_o + R_x + 2 R_y)^2} \right]$$

$$= R_x \frac{(R_z - 1)^2}{R_z + 1} + R_x + \frac{R_x^2 4 R_y R_z^2}{R_x^2 \left(R_z + 1 + \frac{2 R_y}{R_x}\right)^2}$$

$\underbrace{\left(R_z + 1 + \frac{2 R_y}{R_x}\right)^2}_{R_z^2}$

$$= R_x \frac{(R_z - 1)^2}{R_z + 1} + R_x + \frac{4 R_y}{(1 + R_z)^2}$$