1st Order Op Amp Circuits
Objective of Lecture

- Discuss analog computing and the application of 1st order operational amplifier circuits.
- Derive the equations that relate the output voltage to the input voltage for a differentiator and integrator.
- Explain the source of the phase shift between the output and input voltages.
Mechanical Analog Computers

Designed by Vannevar Bush in 1930 and used to control position of artillery through WWII. Replaced by electrical analog computers towards the end of WWII, which performed the needed calculations much faster.

http://www.science.uva.nl/museum/AnalogComputers.html
Why Use an Analog Computer?

- Calculations performed in real time without the use of a ‘real’ computer.
  - Can be integrated into the instrumentation circuitry.
    - Commonly used in control circuits to rapidly monitor and change conditions without the need to communicate back and forth with a digital computer.
    - Power consumption is not high.
- Input can be any value between $V^+$ and $V^-$.  
  - Can be designed to handle large (or small) voltages.
  - No digitizing errors.
- Analog computers are more robust
  - Less susceptible to electromagnetic radiation damage (cosmic rays), electrostatic discharge, electromagnetic interference (pick-up of electric noise from the environment), etc.
Disadvantage

- Slow
  - Maximum frequency is less than 10 MHz
    - Compare this to the clock speed of your digital computer.
  - Voltage transfer function is nonlinear over entire range of input voltages.
  - Timing of inputs needs to be carefully considered.
    - Any time delays can cause errors in the calculations performed.
Subsystems

- **Multipliers**
  - Inverting and non-inverting amplifiers
    - Typically fixed number, which means fixed resistor values in amplifiers

- **Adders and Subtractors**
  - Summing and difference amplifiers

- **Differentiators**
- **Integrators**

\[ \text{1}^{\text{st}} \text{ order op amp circuits} \]
Capacitors

\[ i_C(t) = C \frac{dv_C}{dt} \]

\[ v_C(t) = \frac{1}{C} \int_{t_o}^{t_1} i_C(t) \, dt + v_C(t_o) \]
Differentiator
Ideal Op Amp Model

Virtual ground
Op Amp Model

Virtual ground
Analysis

- Since current is not allowed to enter the input terminals of an ideal op amp.

\[
i_C(t) = i_R(t)
\]

\[
v_C(t) = v_S(t)
\]

\[
i_C(t) = C \frac{dv_C}{dt} = C \frac{dv_S}{dt}
\]

\[
i_R(t) = - \frac{v_o}{R}
\]

\[
- \frac{v_o}{R} = C \frac{dv_S}{dt}
\]

\[
v_o(t) = -RC \frac{dv_S(t)}{dt}
\]
Example #1

- Suppose $v_s(t) = 3V \ u(t-5s)$
  - The voltage source changes from 0V to 3V at $t = 5s$.
    - Initial condition of $V_C = 0V$ when $t < 5s$.
    - Final condition of $V_C = 3V$ when $t > 5RC$. 
Example #1 (con’t)

\[ v_C(t) = 0V \quad \text{when } t < t_o \]
\[ v_C(t) = V_{C_{\text{final}}} + \left( V_{C_{\text{initial}}} - V_{C_{\text{final}}} \right) e^{-\left(t - t_o\right)/\tau} \quad \text{when } t > t_o \]
\[ v_C(t) = 0V + (3V - 0V) e^{-\left(t - 5s\right)/0.8s} \quad \text{when } t > t_o \]
\[ v_C(t) = 3V \, e^{-\left(t - 5s\right)/0.8s} \quad \text{when } t > 5s \]
Example #1 (con’t)

\[ v_o(t) = -RC \frac{dv_c(t)}{dt} \]

\[ v_o(t) = 0V \text{ when } t < 5s \]

\[ v_o(t) = 0V \text{ when } t > t_o + 5\tau, \text{ where } \tau = RC \]

\[ v_o(t) = 0V \text{ when } t > 5s + 5(20k\Omega)(40\mu F) = 9s \]

\[ v_o(t) = \frac{-1}{0.8s} (-20 \times 10^3 \Omega)(40 \times 10^{-6} F)(3V) e^{-(t-5s)/0.8s} \]

\[ v_o(t) = 3V e^{-(t-5s)/0.8s} \]
Example #2

- Let $R = 2 \, k\Omega$, $C = 0.1 \mu F$, $v_s(t) = 2V \sin(500t)$ at $t = 0s$

Since $v_C(t) = v_s(t)$

$v_o(t) = -RC \frac{dv_s}{dt}$

$v_o(t) = -\left(2000\Omega\right)(10^{-7} \, F) \frac{d\left[2V \sin(500t)\right]}{dt}$

$v_o(t) = (-0.2 \, ms)(2V)(500)\cos(500t)$

$v_o(t) = -0.2V \cos(500t)$ when $t > 0s$

$v_o(t) = 0V$ when $t < 0s$
Cosine to Sine Conversion

\[ v_o(t) = -0.2V \cos(500t) \]

\[ v_o(t) = -0.2V \sin(500t + 90^\circ) \]

\[ v_o(t) = 0.2V \sin(500t + 90^\circ - 180^\circ) \]

\[ v_o(t) = 0.2V \sin(500t - 90^\circ) \]

As \( v_s(t) = 2V \sin(500t) \), the output voltage lags the input voltage by 90 degrees.
PSpice Simulation

Shows the 90 degree phase shift as well as the deamplification.

$v_s(t)$  $v_o(t)$
Integrator

Virtual ground
Op Amp Model
Integrator

$$i_R = \frac{v_S(t) - v_1}{R} = \frac{v_S(t)}{R}$$

$$i_C = C \frac{dv_C}{dt}$$

$$v_C(t) = v_1 - v_o(t) = -v_o(t)$$

$$i_R - i_C = 0mA$$

$$\frac{v_S(t)}{R} - C \frac{d[-v_o(t)]}{dt} = 0$$

$$\frac{dv_o(t)}{dt} + \frac{v_S(t)}{RC} = 0$$

$$v_o(t_2) = -\frac{1}{RC} \int_{t_1}^{t_2} v_S(t)dt + v_o(t_1)$$
Example #3

Let \( R = 25 \, k\Omega \), \( C = 5nF \), \( v_s(t) = 3V \sin\left(6.24k \frac{rad}{s} t\right) \) at \( t=0s \)

\[
V_o(t_2) = \frac{-1}{RC} \int_{t_1}^{t_2} V_{in}(t)dt + V_o(t_1)
\]

\[
V_o(t_2) = \frac{-1}{25k\Omega(5nF)} \int_{t_1}^{t_2} 3V \sin\left(6.24k \frac{rad}{s} t\right)dt
\]

\[
V_o(t_2) = 3.85V \cos\left(6.24k \frac{rad}{s} t\right)\bigg|_{t_1}^{t_2} + V_o(t_1)
\]

\[
V_o(t_2) = 3.85V \sin\left(6.24k \frac{rad}{s} t_2 + 90^\circ\right) - 3.85V \text{ when } t_1 = 0s
\]

since \( v_o(t) = -v_C(t) \) and the voltage across a capacitor can't be discontinuous.
PSpice Simulation

Shows that the output voltage leads the input voltage by +90 degree and the voltage offset due to the $V_o(t_1)$ term.
Example #4
Initial Charge on Capacitor
Example #4 (con’t)

If there is an initial charge that produces a voltage on the capacitor at some time, $t_o$:

The voltage on the negative input of the op amp is:

$$v_1 = V_C + V_{R1}$$

$$v_1 = v_2 = 0V$$
Example #4 (con’t)

The current flowing through $R_1$ is the same current flowing through $C$.

$$i_C(t) = C \frac{dv_C(t)}{dt}$$

$$i_{R1}(t) = \frac{V_{R1}}{R_1} = \frac{[v_1 - v_C(t)]}{R_1} = \frac{[0V - v_C(t)]}{R_1} = - \frac{v_C(t)}{R_1}$$

at $t = t_o$, $i_R(t_o) = - \frac{v_C(t_o)}{R_1}$

as $t \to \infty$, $v_C(t) \to 0V, i_C(t) \to 0mA$
\[ i_C(t) - i_{R1}(t) = 0 \]

\[ C \frac{dv_C(t)}{dt} + \frac{v_C(t)}{R_1} = 0 \]

\[ \frac{dv_C(t)}{dt} + \frac{v_C(t)}{R_1C} = 0 \]

\[ v_C(t) = v_C(t_o)e^{-\frac{t-t_o}{R_1C}} \]

\[ i_C = C \frac{dv_C(t)}{dt} = -\frac{1}{R_1} v_C(t_o)e^{-\frac{t-t_o}{R_1C}} \]

\[ R_1C \text{ is the time constant, } \tau. \]
\[ i_{R2} = -i_C \]
\[ i_{R2} = \frac{0V - v_o(t)}{R_2} = -\frac{v_o(t)}{R_2} \]
\[ v_o(t) = \frac{R_2}{R_1} v_C(t_o) e^{-\frac{t-t_o}{R_1C}} \]
Summary

- Differentiator and integrator circuits are 1st order op amp circuits.
  - When the C is connected to the input of the op amp, the circuit is a differentiator.
    - If the input voltage is a sinusoid, the output voltage lags the input voltage by 90 degrees.
      - The output voltage may be discontinuous.
  - When the C is connected between the input and output of the op amp, the circuit is an integrator.
    - If the input voltage is a sinusoid, the output voltage leads the input voltage by 90 degrees.
      - The output voltage must be continuous.